

The ROSAT all-sky survey catalogue of the nearby stars^{*}

M. Hünsch¹, J.H.M.M. Schmitt^{2,4}, M.F. Sterzik^{3,4}, and W. Voges⁴

¹ Institut für Theoretische Physik und Astrophysik, Universität Kiel, Olshausenstrasse 40, 24118 Kiel, Germany

² Hamburger Sternwarte, Universität Hamburg, Gojenbergsweg 112, 21029 Hamburg, Germany

³ European Southern Observatory, Casilla 19001, Santiago 19, Chile

⁴ Max-Planck-Institut für extraterrestrische Physik, Giessenbachstr. 1, 85740 Garching, Germany

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Abstract. We present X-ray data for all entries of the Third Catalogue of Nearby Stars (Gliese & Jahreiß 1991) that have been detected as X-ray sources in the ROSAT all-sky survey. The catalogue contains 1252 entries yielding an average detection rate of 32.9 percent. In addition to count rates, source detection parameters, hardness ratios, and X-ray fluxes we also list X-ray luminosities derived from *Hipparcos* parallaxes.

Key words: stars: activity — stars: coronae — stars: late-type — X-rays: stars

1. Introduction

One of the major results obtained with the imaging X-ray telescopes flown onboard the *Einstein* and ROSAT observatories is the ubiquity of X-ray emission from normal stars throughout the whole Hertzsprung-Russell (HR) diagram, the only exceptions being A-type main sequence stars and some of the late-type giants and supergiants. However, the more sensitive ROSAT observations have revealed X-ray emission even from those types of stars.

X-ray emission from late-type stars is generally attributed to magnetically heated stellar coronae. As suggested by the example of the Sun's corona, the X-ray emitting hot ($> 10^6$ K) plasma is believed to be confined by coronal magnetic fields, which ultimately originate from the interaction between rotation and outer convection zones. The solar X-ray luminosity varies approximately between $3 \cdot 10^{25}$ and $1 \cdot 10^{27}$ erg s⁻¹ (extrapolated to a 1 – 300 Å “bolometric X-ray band”;

cf. Haisch & Schmitt 1996; Acton 1996) during the solar cycle and is known to be strongly correlated with other magnetic activity indicators (e.g., sunspot numbers, flare frequency, chromospheric Ca II emission). Hence, X-ray luminosity can be regarded as a good activity indicator also for other late-type stars. Conversely, X-ray emission from O- and early B-type stars obeys (approximately) a $L_x/L_{\text{bol}} \approx 10^{-7}$ relation and is attributed to shocks generated and dissipated within the radiatively driven winds of those stars.

A thorough investigation of the properties of stellar X-ray emission requires large samples of stars in order to reduce the effects of individual scatter and to construct samples of stars with given properties such as mass, age, rotation rate etc. Especially important are complete, volume-limited samples of stars, for example, to derive X-ray luminosity distribution functions. In principle, there are two different approaches: i) to construct such a complete sample and to look for X-ray emission from those stars afterwards, and ii) to scan the whole sky for X-ray emission and then to extract the data for the sample stars (input positions). The first method has been applied by Schmitt et al. (1995) and Schmitt (1997) for the immediate solar environment, i.e., the K- and M-type stars within 7 pc and the A-, F-, and G-type stars within 13 pc from the Sun, respectively. These investigations revealed that virtually every late-type dwarf star with spectral type later than A7 can be detected as an X-ray source given data of sufficient sensitivity. These data are from both the ROSAT all-sky survey (RASS) and deep individual pointed ROSAT observations. A similar investigation on late-type giants within 25 pc has been performed by Hünsch et al. (1996).

The second method requires the existence of a sufficiently deep all-sky survey. Until now, the ROSAT observatory has undertaken the only sensitive X-ray survey. These data provide a flux-limited but otherwise unbiased sample of X-ray sources (Voges et al. 1996a). Of the $\approx 1.5 \cdot 10^5$ detected sources, about one third are

Send offprint requests to: M. Hünsch,
e-mail: huensch@astrophysik.uni-kiel.de

^{*} Catalogue also available at CDS via anonymous ftp to cdsarc.u-strasbg.fr (130.79.128.5) or via <http://cdsweb.u-strasbg.fr/Abstract.html>

considered to be coronal. We used these data to search for X-ray emission from stars contained in the Catalogue of Nearby stars (the so-called Gliese catalogue; Gliese & Jahreiß 1991). The Gliese catalogue is the most comprehensive list of stars in the solar environment and it is proposed to be as complete as possible within a space volume of 25 pc radius around the Sun. Our investigation is limited in completeness by both the completeness of the Gliese catalogue and the sensitivity of the RASS. However, also for those Gliese stars that are not detected, it is in principle possible to estimate upper limits for their X-ray luminosity (see Sect. 2.1).

A preliminary investigation of stellar activity of the nearby stars based on the data presented here has already been performed by Sterzik & Schmitt (1997). However, X-ray luminosities for those stars derived from ROSAT data combined with *Hipparcos* parallaxes are presented here for the first time.

We have also performed similar surveys of X-ray emission from the stars contained in the Bright Star catalogue (BSC; Hoffleit & Warren 1991). These results are presented as catalogues of X-ray data, which have already been published for OB stars (Berghöfer et al. 1996), late-type giants and supergiants (Hünsch et al. 1998a; hereafter HSV98), and late-type main-sequence stars and subgiant stars (Hünsch et al. 1998b).

2. RASS data and detection of late-type stars

2.1. The ROSAT all-sky survey (RASS)

During its first half year of operations, the ROSAT observatory carried out the first all-sky survey with an imaging X-ray telescope between July 1990 and January 1991. Further survey observations were carried out in February 1991 (2 days) and August 1991 (10 days). The whole sky was scanned along great circles perpendicular to the direction to the Sun. Because of the Earth's motion around the Sun, the plane of these circles slowly ($1^\circ/\text{d}$) rotated around an axis through the ecliptic poles, thus covering the whole celestial sphere within 6 months. Each point of the sky was observed several times as the scan paths of 2 degrees width (i.e., the field of view of the PSPC detector) progressed along the ecliptic. Therefore, the data of any particular source consist of a number of "snapshots" of up to 30 s duration, separated by the orbital period of the satellite (≈ 90 min) and distributed over an interval of at least 2 days. Towards the ecliptic poles, the cumulative exposure time increases due to the larger number of scans covering a particular celestial position. Depending on the ecliptic latitude (and down-time due to passages through the radiation belts of the Earth), the effective exposure time varies between ~ 100 s and $\sim 40\,000$ s (at the poles), with typical values of ~ 400 s at the ecliptic. Typical limiting RASS count rates are ≈ 0.015 ctss $^{-1}$;

given a typical energy-conversion factor for soft sources of $6 \cdot 10^{-12}$ erg cts $^{-1}$ cm $^{-2}$ (cf. Sect. 2.3) the typical detection limit of RASS observations amounts to a limiting flux of $f_x \approx 10^{-13}$ erg cm $^{-2}$ s $^{-1}$. At the distance limit of the Gliese catalogue, i.e., at 25 pc, this corresponds to an X-ray luminosity of $L_x \approx 7.5 \cdot 10^{27}$ erg s $^{-1}$. Note that this is not an average value for the detection limit for the Gliese stars since many stars are closer and the exposure time increases towards the ecliptic poles.

For a more detailed description of the RASS we refer to Voges (1992) and Belloni et al. (1994). Details of the ROSAT observatory in general can be found in Trümper (1983) and Trümper et al. (1991). The PSPC detector used during the RASS is described by Pfeffermann et al. (1986). In February 1997 the remaining gaps left in the all-sky survey were filled with a sequence of more than 500 pointed, partially overlapping PSPC observations so that with the exception of a small region around the strong X-ray source Sco X-1 the whole sky has been imaged with the ROSAT PSPC. In the catalogue presented in this paper we include sources detected in this "survey repair" pointed observations; they are marked with an asterisk.

The source detection was performed by means of a maximum likelihood algorithm (Cruddace et al. 1988) in the course of the standard analysis software system (SASS; Voges et al. 1992). The significance of an X-ray source is expressed by the likelihood $\text{Li} = -\ln(1-P)$, where P is the probability of existence; e.g., a likelihood of $\text{Li} = 7$ corresponds to a source existence probability of 99.9%. The result of the SASS is a comprehensive list of approximately 10^5 sources, each described by the sky position in right ascension and declination, its source detection likelihood, count rate, hardness ratios, extent, and corresponding errors. The data for the brighter X-ray sources have been released as the ROSAT All-sky Survey Bright Source Catalogue (Voges et al. 1996b), which contains sources with Likelihood ≥ 15 , count rate larger than 0.05 s $^{-1}$, and with at least 15 detected photons.

2.2. Identification of X-ray sources with nearby stars

We used the Third Catalogue of Nearby Stars (Gliese & Jahreiß 1991) as input sample for our search of X-ray bright nearby stars. That input sample consists of 3802 stars.

The procedure whereby the positions of RASS sources were matched with the stars of our input sample is the same as described in HSV98. We accepted sources with a likelihood greater than or equal to 7 within 90 arcsec distance from the input stars. As for the BSC sample, the choice of this cut-off radius is empirically justified by means of a Monte Carlo simulation of about the same number of random positions as input positions. However, since the binary fraction is much larger in the Gliese catalogue than in the BSC, the number of independent input

positions is significantly smaller than the total number of catalogue entries; we therefore combined all binaries into one input position for each system, since most of them are too close to be separated with the RASS data. This results in only 3365 independent input positions, for which we determined the distribution of offsets. The same number of random positions results in 112 (artificial) matches with X-ray sources, yielding a mean of $1.1 \cdot 10^{-3}$ matches per square arcsec in the offset distribution plane, i.e., about one third of that of the random sample used for the 9110 BSC stars (as expected). At 90 arcsec offset the number of matches of X-ray sources with real stars exceeds the number of artificial matches by a factor of 2. That means, at 90 arcsec offset between optical and X-ray position the differential probability that the X-ray source can be attributed to the star (and not to a background object) is 50%. This differential probability increases very rapidly for smaller values of positional offset, while for even larger values of offset the chance for obtaining a spurious identification exceeds that of finding the true X-ray counterpart.

We note that the accuracy of the input positions in the Gliese catalogue (given only to integers of seconds in RA and tenth of arcminutes in Dec) is less than for the BSC stars, hence resulting in a somewhat broader distribution of the offsets for the real stars. On the other hand, the intrinsic detection probability is larger for the Gliese stars than for the BSC stars because the Gliese stars are closer to us and the content of late-type stars is much larger. This would cause a somewhat steeper distribution of the offsets. Probably, both effects compensate each other, thus leading to a 50% differential probability for a correct identification at essentially the same offset value.

Of the X-ray sources extracted by the match procedure, 469 are rather weak sources that are not included in the Bright Source Catalogue (Voges et al. 1996b). We checked their X-ray images by eye for reality. Specifically, we rejected photon distributions that are significantly contaminated by nearby strong sources or that are obviously extended. In questionable cases, we ran the standard source detection algorithm of EXSAS on the source images in different passbands and decided on the basis of the results which sources to retain in our final catalogue.

Confining now attention to the 3365 (independent) input positions identified with Gliese stars, we detected X-ray emission from 1252 stars, i.e., the average detection rate is 37%. Since the total search area around these 3365 stars is $3365 \cdot \pi \cdot (1.5')^2 = 6.61 \square^\circ = 0.016\%$ of the sphere, and the total number of RASS sources amounts to $\sim 150\,000$, we would expect 24.0 chance coincidences of Gliese stars with background (or foreground) X-ray sources (i.e., 1.92% of our detected sources).

2.3. Determination of X-ray fluxes and luminosities

The procedure of determining X-ray fluxes has also been described in HSV98. In this paper, we followed the same procedure, except using a slightly different formula for the calculation of individual energy-conversion factors

$$\text{ECF} = (5.30 \cdot HR + 8.31) 10^{-12} \text{ erg cm}^{-2} \text{ cts}^{-1} \quad (1)$$

which was derived by Schmitt et al. (1995) from an X-ray study of a complete sample of main-sequence stars within 7 pc distance; here HR denotes the hardness ratio defined through

$$HR = \frac{H - S}{H + S}, \quad (2)$$

where H and S denote the source counts in the hard (0.5–2.0 keV) and soft (0.1–0.4 keV) passbands of ROSAT. The hardness ratio is an “X-ray color” that is influenced by both the plasma temperature and the hydrogen column density.

Since the SASS source detection was separately performed in both passbands and since most of our X-ray sources were detected in both bands, the hardness ratios can be estimated for many stars, although in some cases with quite substantial errors. In a few cases, when the sources were not detected in either the soft or the hard passband, we set $HR = +1.0$ or -1.0 by definition, respectively. We refrain from estimating individual errors for f_x since the error in ECF is very difficult to quantify. In general, we estimate this error to be within a factor of two for the weaker sources and less for the brighter sources.

The X-ray luminosities are calculated by the relation

$$L_x = 4\pi d^2 \times f_x, \quad (3)$$

where d is the distance to the star. We used the distances revised on the basis of the *Hipparcos* parallaxes (ESA 1997) and kindly made available to us by H. Jahreiß. No X-ray luminosities are computed for those few stars for which no reliable distances exist. Note that the catalogue contains a few stars which obviously do not belong to the solar environment but were erroneously included in the third version of the Gliese catalogue.

3. The catalogue

The table contains optical and X-ray data of all 1252 detected Gliese stars. Note that many entries are actually binaries. In a few cases, both components have been detected separately. However, in most cases, the detected X-ray source is attributed to both components and no attempt is made to split up the X-ray flux. As a consequence, care must be taken when interpreting the catalogue information for binaries. For example, in the case of Gl 244 A, B (= Sirius), the X-ray flux is known to arise exclusively from the hot white dwarf B-component, while in the

case of Gl 280 A, B (= Procyon) the X-ray emission comes from the late-type primary component. In our catalogue, however, the same X-ray flux is attributed to the A- as well as the B-components.

Also note that the quoted count rates are mean count rates during the survey observations, computed as the ratio of total number of counts and integrated exposure time. In some cases, these numbers can strongly be affected by individual flare events (e.g., Gl 877 = EV Lac, see Schmitt 1994; see also Haisch & Schmitt 1994).

The columns of the table contain the following information:

Column 1: Designation of catalogue entry. Where available, we prefer the original Gliese (Gl), Gliese-Jahreiß (GJ), or Woolley (Wo) designation. Stars without such a number are named according to one of the following other catalogues (in hierarchical order): Henry Draper (HD), Giclas (G), Luyten Half Second (LHS), Durchmusterung (BD or CD), or various other designations (LTT, LP, GR, Steph, Rob, BPM, AC). Only in very few cases, where we did not find any common designation, do we use the approximate celestial position instead. Stars marked with an asterisk were detected in the “survey repair” observations (cf. Sect. 2.1).

Column 2: V magnitude (from Gliese catalogue).

Column 3: $B - V$ color index (from Gliese catalogue).

Column 4: MK spectral classification (from Gliese catalogue).

Column 5: Distance to the star as given by the *Hipparcos* parallaxes.

Column 6: effective exposure time in seconds.

Column 7: mean PSPC count rate in counts per second.

Column 8: error of PSPC count rate.

Column 9: likelihood of existence (cf. Sect. 2.1); a value of 999 indicates a source existence likelihood of 999 or greater.

Column 10: offset in arcsec between optical and X-ray position.

Column 11: hardness ratio $HR = (H - S)/(H + S)$ (cf. Sect. 2.3).

Column 12: error of hardness ratio.

Column 13: apparent X-ray flux (0.1 – 2.4 keV) in 10^{-14} erg cm $^{-2}$ s $^{-1}$ (see Sect. 2.3).

Column 14: X-ray luminosity derived from the distance as given in Col. 5. The values are given in units of 10^{27} erg s $^{-1}$.

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Name	<i>V</i>	<i>B</i> - <i>V</i>	Sp. type	<i>d</i> (pc)	Exp.	<i>CR</i>	$\pm CR$	Li	Δ	<i>hr</i>	Δhr	<i>f</i> _{x-14}	<i>L</i> _{x27}
HD 225239	6.11	0.62	G2 V	36.8	262	0.628	0.052	489	1	-0.27	0.08	432.3	699.2
Gl 1	8.54	1.46	M4 V	4.4	156	0.059	0.024	9	26	-0.68	0.29	27.9	0.6
Gl 4 A	8.97	1.44	dK6 e	11.8	380	0.049	0.014	24	7	-0.42	0.25	30.1	5.0
Gl 4 B	9.02	1.45	M0.5 V	11.8	380	0.049	0.014	24	6	-0.42	0.25	30.1	5.0
Gl 4.1A	6.43	0.64	G5 V	20.3	508	0.323	0.026	409	4	-0.33	0.08	212.0	104.4
Gl 4.1B	7.20	0.78	dG8	20.3	508	0.323	0.026	409	4	-0.33	0.08	212.0	104.4
Gl 5	6.14	0.75	K0 Ve	13.7	327	0.687	0.048	624	4	-0.22	0.07	490.6	110.2
G131-026	13.54		m	10.3	251	0.090	0.021	38	5	-0.28	0.21	61.4	7.8
Gl 8	2.27	0.34	F2 III-IV	16.7	496	0.162	0.020	153	6	-0.55	0.10	87.7	29.2
G243-016	9.48	1.22	K7	28.0	467	0.026	0.009	14	25	-0.54	0.30	14.1	13.2
G242-048	11.12	1.50	M1.5	19.6	836	0.028	0.007	23	12	-0.25	0.26	19.5	8.9
G242-048	17.40		m	19.6	836	0.028	0.007	23	15	-0.25	0.26	19.5	8.9
GR 4	14.31	1.57	dM3.4		120	0.037	0.020	8	4	-0.98	1.05	11.6	
GJ 1006 A	12.27	1.50	M4	15.1	342	0.350	0.033	287	10	-0.28	0.09	239.2	65.5
GJ 1006 B	13.22	1.60	M4.5	15.1	342	0.350	0.033	287	23	-0.28	0.09	239.2	65.5
HD 1237	6.60		G6 V	17.6	231	0.388	0.045	194	5	-0.21	0.11	279.5	103.6
G131-047	13.77		m	20.8	373	0.047	0.013	27	12	-0.27	0.26	32.4	16.8
Gl 14	9.00	1.36	dM0.5	15.0	336	0.052	0.014	30	11	-0.45	0.23	30.9	8.3
G158-052	11.00	1.42	dM0	35.2	356	0.034	0.012	13	25	-0.83	0.23	13.1	19.5
Gl 15 A	8.08	1.56	M2 V	3.6	453	0.260	0.026	202	18	-0.66	0.08	125.2	1.9
Gl 15 B	11.06	1.79	M6 Ve	3.6	453	0.260	0.026	202	18	-0.66	0.08	125.2	1.9
LHS 5004a	12.29	1.46	M3:	20.0	209	1.001	0.071	633	49	-0.17	0.07	741.6	353.5
LP 149-56	12.84		m	21.6	513	0.074	0.014	55	10	-0.26	0.16	51.1	28.5
Gl 17.2	8.30	0.90	K3 V	27.4	239	0.051	0.018	11	22	-0.26	0.34	35.1	31.6
Gl 17.3	6.38	0.66	G2 V	20.4	321	0.289	0.033	209	12	-0.29	0.10	195.7	97.5
GJ 1010 A	11.30	1.49	k-m	19.7	914	0.011	0.004	10	14	-0.61	0.33	5.7	2.7
GJ 1010 B	14.00		m	19.7	914	0.011	0.004	10	23	-0.61	0.33	5.7	2.7
GJ 2004	8.75	1.07	K3/4 V	22.2	328	0.033	0.012	13	11	-1.00	0.64	9.8	5.8
G130-068	14.54	1.67	m	18.9	321	0.065	0.016	38	13	-0.43	0.22	39.1	16.8
GJ 2005	15.42		M5.5	7.4	212	0.053	0.018	13	62	-0.56	0.27	28.3	1.8
Gl 19	2.80	0.62	G2 IV	7.5	195	0.070	0.023	15	21	-1.00	0.41	21.0	1.4
G172-001	13.15		m	13.4	523	0.232	0.023	232	8	-0.24	0.09	163.4	35.2
Gl 22 AC	10.38	1.54	dM2.5e	10.1	304	0.085	0.020	33	18	-0.44	0.18	50.6	6.2
Gl 22 B	12.40		dM3.5	10.1	304	0.085	0.020	33	18	-0.44	0.18	50.6	6.2
LP 525-39	12.70		m	11.8	133	0.287	0.050	77	13	0.01	0.18	240.0	39.9
Gl 22.2	5.57	0.46	F3 IV-V	25.6	216	0.037	0.015	12	40	-1.00	2.36	11.1	8.8
Gl 23 A	5.65	0.57	F6 V	21.1	421	1.116	0.076	588	8	-0.21	0.07	803.2	425.9
Gl 23 B	6.40		G1 V	21.1	421	1.116	0.076	588	8	-0.21	0.07	803.2	425.9
HD 3302	5.51	0.44	F6 V	36.2	184	0.224	0.039	61	19	-0.22	0.16	160.2	251.7
Gl 24 A	6.79	0.64	G3 V	43.9	231	0.327	0.039	168	5	-0.37	0.12	207.8	478.3
Gl 28	7.36	0.94	K2 Ve	17.3	485	0.026	0.009	13	30	-0.45	0.31	15.4	5.5
Gl 29.1	10.52	1.50	dM0 e	23.8	464	1.022	0.047	999	5	-0.21	0.05	735.5	498.9
Gl 31	2.04	1.01	K1 IIIe	29.4	313	2.649	0.165	835	1	0.28	0.06	2594.4	2685.2
Gl 31.3	5.23	0.34	F2 V	27.9	338	0.217	0.028	144	13	-0.07	0.12	172.3	159.9
Gl 32 A	8.41	1.17	K5 V	16.0	296	0.037	0.014	8	36	0.04	0.42	31.2	9.6
Gl 32 B	9.06	1.27	K7 V	16.0	296	0.037	0.014	8	38	0.04	0.42	31.2	9.6
GJ 1021	5.80	0.64	G5 IV	14.9	215	0.335	0.044	130	8	-0.39	0.11	208.9	55.8
Gl 33	5.74	0.88	K2 V	7.5	353	0.043	0.013	17	31	-1.00	0.20	13.0	0.9
Gl 34 A	3.45	0.57	G3 V	6.0	381	0.138	0.022	71	12	-0.72	0.11	62.0	2.6
Gl 34 B	7.51	1.39	K7 V	6.0	381	0.138	0.022	71	12	-0.72	0.11	62.0	2.6
LP 193-584	13.06		m	19.3	185	0.222	0.037	80	24	-0.24	0.17	156.5	69.8
Gl 34.1	5.07	0.51	F8 V	23.9	418	0.024	0.009	11	12	-0.73	0.29	10.6	7.3
Gl 36	7.16	0.78	G9 V	18.8	311	0.034	0.012	11	33	-0.90	0.24	12.1	5.2
Gl 37	5.17	0.50	F7 IV-V	15.5	565	0.073	0.013	54	4	-0.72	0.12	32.7	9.4
LTT 10301	12.70		m	12.0	147	0.443	0.058	187	6	-0.21	0.13	319.2	55.2
LP 350-19	13.30		m	12.0	147	0.443	0.058	187	6	-0.21	0.13	319.2	55.2
Gl 39	9.24	1.21	dK6	21.9	403	0.023	0.009	13	8	0.58	0.35	26.4	15.1
Gl 41	4.82	0.53	F8 V	18.6	326	0.044	0.014	12	29	-0.71	0.24	19.9	8.2
Gl 42	7.17	0.93	K3 V	14.1	337	0.052	0.016	14	13	-0.63	0.18	26.0	6.2
Gl 42.1	7.38	0.65	G5	29.5	108	0.064	0.030	9	41	-0.66	0.62	30.6	31.8
Gl 47	10.83	1.57	dM2.5e	11.0	407	0.031	0.011	16	23	-0.80	0.28	12.7	1.8
Gl 48	10.04	1.46	dM3.5e	8.1	650	0.013	0.006	9	22	-0.90	0.61	4.7	0.4
Gl 51	13.66	1.68	M5	10.5	416	0.227	0.026	179	16	-0.20	0.11	164.8	21.6
GJ 1026 A	11.88		M1.5	16.3	291	0.146	0.024	98	9	-0.27	0.15	100.6	32.1
GJ 1026 B	12.40		M3.5	16.3	291	0.146	0.024	98	9	-0.27	0.15	100.6	32.1
LP 467-16	14.36		m	8.8	345	0.094	0.018	62	7	-0.08	0.20	73.8	6.8
Gl 54.1	12.05	1.84	dM5 e	3.7	461	0.254	0.026	200	15	-0.19	0.10	185.4	3.1
HD 7205	7.28	0.78	G5	44.6	385	0.269	0.029	247	4	-0.10	0.10	209.6	499.8
GJ 1033	14.16	1.58		17.4	287	0.071	0.018	37	20	-0.16	0.25	52.8	19.1
Gl 54.2A	5.14	0.45	F5 V	24.4	335	0.126	0.021	84	11	-0.01	0.16	104.0	74.0
Gl 54.2B	7.85	0.78	K1 V	24.4	335	0.126	0.021	84	55	-0.01	0.16	104.0	74.0
Gl 55	4.96	0.58	F8 V	15.1	324	0.039	0.013	16	9	-1.00	0.98	11.6	3.2
Gl 55.1A	7.80	0.98	K2 V	21.1	107	0.115	0.039	13	25	-0.11	0.31	89.1	47.4
Gl 55.1B	8.20			21.1	107	0.115	0.039	13	25	-0.11	0.31	89.1	47.4
Gl 55.3A	4.99	0.47	F6 IV	20.4	110	0.522	0.072	116	15	-0.40	0.13	322.9	161.6
Gl 55.3B	7.20		G5	20.4	110	0.522	0.072	116	10	-0.40	0.13	322.9	161.6
G269-139	14.20		m	24.3	424	0.066	0.017	13	54	-0.14	0.30	49.9	35.2
Gl 56.5	7.11	0.82	dK0	16.8	786	0.014	0.005	9	29	-0.49	0.32	7.9	2.7
HD 8357	7.33		G5	45.2	396	4.673	0.358	546	5	-0.17	0.08	3462.2	8481.2
Gl 57.1A	7.85	0.90	K0 IV	30.2	390	0.022	0.009	10	9	-0.89	0.25	8.0	8.8

Name	V	$B - V$	Sp. type	$d(\text{pc})$	Exp.	CR	$\pm CR$	Li	Δ	hr	Δhr	f_{x-14}	L_{x27}
Gl 57.1B	10.38	1.38	dK7	30.2	390	0.022	0.009	10	46	-0.89	0.25	8.0	8.8
Gl 57.1C	13.10			30.2	390	0.022	0.009	10	46	-0.89	0.25	8.0	8.8
Gl 58.2	7.73	0.96	K2 V	23.1	436	0.105	0.017	69	8	-0.41	0.14	64.4	41.3
Gl 59 A	6.97	0.76	G8 V	19.5	251	0.059	0.019	19	4	-0.80	0.17	24.1	10.9
Gl 60 A	7.78	0.92	K3 V	23.6	486	2.594	0.209	389	6	-0.20	0.08	1880.7	1257.5
Gl 60 B	8.00		K4 V	23.6	486	2.594	0.209	389	6	-0.20	0.08	1880.7	1257.5
Gl 60 C	10.40		M2 V	23.6	486	2.594	0.209	389	6	-0.20	0.08	1880.7	1257.5
Gl 61	4.09	0.54	F8 V	13.5	354	0.135	0.023	66	33	-0.71	0.11	61.3	13.3
LHS 1268	10.50		K7	21.8	257	0.142	0.027	57	30	-0.03	0.19	115.6	65.9
Gl 65 A	12.57	1.85	dM5.5e	2.7	484	0.680	0.057	318	11	-0.32	0.08	450.0	3.9
Gl 65 B	12.70		dM5.5e	2.7	484	0.680	0.057	318	11	-0.32	0.08	450.0	3.9
Gl 65.2	9.86	1.16	M0	40.2	423	0.022	0.010	9	29	-0.78	0.24	9.2	17.7
Gl 67.1	5.88	0.61	G2 V	27.1	291	0.260	0.032	156	6	-0.09	0.12	203.3	178.7
Gl 69	8.41	1.22	K5 V	13.4	533	0.056	0.012	49	15	-0.41	0.19	34.6	7.5
Gl 71	3.49	0.72	G8 Vp	3.6	445	0.052	0.013	24	14	-1.00	0.09	15.6	0.2
Gl 75	5.63	0.81	K0 V	10.0	572	0.360	0.026	505	6	-0.60	0.06	184.8	22.0
W ₀ 9061 A	4.67	0.33	F3 III	23.6	454	0.248	0.025	211	4	-0.39	0.09	155.0	103.7
W ₀ 9061 B	6.77	0.62	dG1	23.0	450	0.386	0.032	430	5	-0.39	0.07	241.0	152.4
G159-003	14.60		m	10.7	230	0.050	0.018	15	19	-0.36	0.29	32.0	4.4
Gl 78.1	3.42	0.48	F6 IV	19.6	284	1.005	0.062	875	11	-0.05	0.06	808.5	373.4
HD 11373	8.48	1.01	G5	22.1	509	0.040	0.010	29	25	-0.11	0.25	30.9	18.1
Gl 79	8.90	1.41	K5/M0 V	11.1	395	0.070	0.016	34	14	-0.30	0.20	47.0	6.9
Gl 81 A	3.70	0.85	G5 IV	17.5	280	1.660	0.115	579	3	0.00	0.07	1379.5	504.4
Gl 81 B	10.70			17.5	280	1.660	0.115	579	3	0.00	0.07	1379.5	504.4
Gl 82	12.21	1.56	dM4 e	12.0	583	0.457	0.029	670	6	-0.23	0.06	323.8	56.0
GJ 1041 A	10.98	1.52	k-m	29.9	387	0.324	0.031	261	8	-0.24	0.09	227.8	242.9
GJ 1041 B	14.00		m	29.9	387	0.324	0.031	261	8	-0.24	0.09	227.8	242.9
Gl 83	2.86	0.28	F0 V	21.9	378	0.055	0.015	21	4	-1.00	0.08	16.6	9.5
G245-040	14.12	1.90	m	9.5	765	0.044	0.009	38	20	-0.48	0.16	25.4	2.7
Gl 83.1	12.28	1.80	dM8 e	4.4	295	0.167	0.025	111	7	-0.27	0.15	115.2	2.7
G272-137	14.10		m	24.2	325	0.025	0.010	11	32	-0.47	0.29	14.4	10.1
G003-035	14.27		dM5 :	16.8	289	0.126	0.023	70	5	-0.42	0.17	76.6	25.7
HD 12545	8.36		G5	196.1	117	0.995	0.096	247	3	0.36	0.09	1017.2	46790.3
Gl 83.4A	7.31	0.69	G3 V	49.3	471	0.431	0.032	442	2	0.12	0.07	385.1	1118.1
Gl 83.4B	11.50			49.3	471	0.431	0.032	442	2	0.12	0.07	385.1	1118.1
HD 12786	7.78		K0 V	25.5	234	0.100	0.024	30	18	0.31	0.24	99.2	77.3
Gl 84	10.19	1.51	M3	9.4	374	0.077	0.017	38	24	-0.52	0.18	42.9	4.6
G244-049	14.31		m	19.3	522	0.088	0.015	61	13	-0.25	0.16	61.3	27.3
*G173-039	12.47	1.54	M5 :	14.2	694	0.210	0.017	489	10	-0.26	0.07	145.9	35.2
Gl 86	6.12	0.82	K0 V	10.9	375	0.058	0.016	24	28	-0.64	0.19	28.6	4.1
Gl 87.1A	5.67	0.56	F8 V	46.1	345	0.031	0.012	8	30	-0.47	0.32	17.9	45.5
Gl 87.1B	7.74	0.68	G5 V	25.6	345	0.031	0.012	8	45	-0.47	0.32	17.9	14.1
G159-046	13.50		m	14.1	316	0.085	0.019	42	7	-0.24	0.21	59.6	14.2
GJ 1044	9.88	1.36	K7 V	23.3	278	0.024	0.011	7	50	0.17	0.54	21.8	14.1
Gl 90	7.09	0.90	K2 V	18.1	672	0.045	0.009	44	3	-0.62	0.14	22.8	9.0
GJ 1045	14.44	1.62	m+	20.5	184	0.019	0.011	8	67			16.0	8.1
G074-011	13.58		m	18.0	270	0.044	0.017	9	38	-0.20	0.35	31.8	12.2
Gl 91.2A	8.42	1.02	K3 V	22.2	389	0.084	0.017	40	13	-0.28	0.18	57.6	34.0
Gl 91.2B	9.10		K	22.2	389	0.084	0.017	40	13	-0.28	0.18	57.6	34.0
LHS 1375	15.79	1.98	m	8.5	229	0.035	0.014	14	41	-0.52	0.43	19.3	1.7
Gl 92	4.87	0.61	G0 Ve	10.8	299	0.423	0.039	285	8	-0.38	0.09	266.6	37.5
LHS 1377	12.00		M4	14.2	481	0.242	0.024	189	11	-0.52	0.08	134.6	32.7
G035-040	14.17		m	22.8	200	0.057	0.021	15	29	0.33	0.35	57.5	35.7
HD 14629	8.74	1.04	K3/4 V	25.4	517	0.021	0.009	9	5	-0.35	0.31	13.9	10.8
Gl 96	9.41	1.49	dM1.5e	11.9	563	0.031	0.009	19	17	-0.58	0.22	16.2	2.8
Gl 97	5.20	0.60	G1 V	21.9	266	0.869	0.060	726	11	-0.08	0.07	685.5	394.4
G074-025	14.05		m	19.6	305	0.050	0.015	16	11	-0.50	0.28	28.3	13.1
HD 15814	6.02	0.54	F8 V	28.7	122	0.306	0.055	58	19	-0.39	0.16	191.3	189.0
Gl 102	12.96	1.70	M4	9.8	246	0.145	0.027	51	15	-0.52	0.15	80.6	9.2
Gl 103	8.85	1.39	K7 Ve	11.5	460	2.705	0.224	360	11	0.17	0.08	2491.6	394.8
02 32 30 +23 21.	13.71	1.58	M3 e	18.2	243	0.098	0.023	34	40	-0.42	0.21	59.7	23.7
Gl 105 A	5.82	0.98	K3 V	7.2	232	0.058	0.019	19	15	-0.66	0.20	28.1	1.7
GJ 1048	8.43	1.08	K2 V	21.3	338	0.036	0.013	16	15	-0.11	0.35	27.7	15.0
G074-034	13.63		M3	15.3	317	0.048	0.015	20	22	-0.70	0.20	22.3	6.3
LTT 10855	13.90		M3.5	15.3	317	0.048	0.015	20	22	-0.70	0.20	22.3	6.3
W ₀ 9087	8.10	0.95	K3	24.3	105	0.115	0.038	17	64	-0.07	0.31	91.7	64.9
02 34 24 +06 41.	16.00		M5 e	20.3	226	0.034	0.016	9	73	-0.15	0.43	25.9	12.8
Gl 105.1	5.78	0.65	G5 IV	25.5	448	0.028	0.010	12	4	-1.00	0.22	8.4	6.5
G076-019	14.27		m	20.7	243	0.054	0.018	14	5	-0.09	0.33	42.3	21.6
Gl 105.4A	5.50	0.44	F5 V	27.0	256	0.053	0.018	13	7	-0.45	0.28	31.2	27.2
Gl 105.4B	5.60		F5 V	27.0	256	0.053	0.018	13	7	-0.45	0.28	31.2	27.2
GJ 1049	9.65	1.39	M0 Ve	16.5	272	1.337	0.073	938	4	-0.21	0.05	962.2	314.5
HD 16673	5.78	0.52	F8 V	21.6	225	0.156	0.030	54	16	-0.81	0.10	62.6	34.8
Gl 105.6	4.92	0.59	F9 V	24.7	558	0.034	0.010	15	23	-0.57	0.26	17.8	13.0
Gl 106	8.28	1.07	dK4	18.6	302	0.081	0.019	40	16	-0.20	0.21	58.7	24.2
Gl 106.1A	3.56	0.09	A3 V	25.1	224	0.376	0.044	159	20	-0.12	0.12	288.8	218.2
Gl 106.1B	6.30		dF3	25.1	224	0.376	0.044	159	20	-0.12	0.12	288.8	218.2
Gl 107 A	4.13	0.49	F7 V	11.2	527	0.152	0.019	140	6	-0.70	0.08	70.1	10.6
Gl 107 B	10.06	1.48	M1 V	11.2	527	0.152	0.019	140	6	-0.70	0.08	70.1	10.6
Gl 108	5.41	0.56	G3 IV	17.2	825	0.281	0.045	70	9	-0.29	0.14	190.5	67.8

Name	V	$B - V$	Sp. type	$d(\text{pc})$	Exp.	CR	$\pm CR$	Li	Δ	hr	Δhr	f_{x-14}	L_{x27}
GI 109	10.57	1.56	dM3.5	7.6	399	0.053	0.014	23	17	-0.51	0.27	29.6	2.0
HD 17169	7.12		G5 V	107.5	401	0.098	0.018	67	10	0.18	0.18	90.4	1250.8
*Wo 9099	4.27	0.31	F0 IV	25.8	1263	0.101	0.009	295	21	-0.64	0.07	49.7	39.7
GI 111	4.46	0.48	F6 V	14.0	288	0.906	0.059	559	11	-0.23	0.06	642.7	150.0
GI 113 AB	7.61	0.83	K1 Ve	22.4	280	0.116	0.023	54	18	-0.26	0.17	80.8	48.4
GI 113 C	16.50		m	22.4	280	0.116	0.023	54	24	-0.26	0.17	80.8	48.4
GI 113.1	6.76	0.96	G9 e	44.1	169	6.792	0.202	999	6	-0.08	0.03	5356.2	12436.3
LP 298-42	13.96		m	16.2	229	0.041	0.016	14	16	-0.50	0.32	22.9	7.2
GI 117	6.03	0.87	K2 V	10.4	220	1.200	0.077	883	13	-0.11	0.06	927.2	119.6
HD 17948	5.59	0.45	F4 V	26.5	550	0.028	0.009	18	32	-1.00	0.26	8.5	7.1
GI 118.1A	8.23	0.93	K3 V	29.6	408	0.073	0.016	34	12	-0.65	0.14	35.3	37.0
GI 118.1B	13.10	1.52	M3 :	29.6	408	0.073	0.016	34	25	-0.65	0.14	35.3	37.0
GI 120.1A	8.03	0.87	K1/2 V	22.5	262	0.029	0.012	10	24	-1.00	1.23	8.7	5.3
GI 120.1B	8.20			22.5	262	0.029	0.012	10	24	-1.00	1.23	8.7	5.3
GI 120.1C	7.83	0.95	K2 V	25.7	262	0.029	0.012	10	21	-1.00	1.23	8.7	6.9
GI 120.2	6.62	0.72	G8 V	21.1	592	0.020	0.008	10	33	-1.00	0.20	6.0	3.2
LTT 1445	10.96	1.69	M3	7.6	211	0.177	0.033	57	26	-0.54	0.15	96.4	6.7
LP 771-96	11.80		M3	7.6	211	0.177	0.033	57	26	-0.54	0.15	96.4	6.7
GI 124	4.05	0.60	G0 V	10.5	523	0.021	0.007	13	57	-1.00	0.89	6.4	0.9
GJ 1054 A	10.24	1.41	K7 V	19.1	227	1.538	0.086	999	8	-0.28	0.05	1049.8	457.5
GJ 1054 B	13.09	1.64	m+	19.1	227	1.538	0.086	999	65	-0.28	0.05	1049.8	457.5
CD-25 1273	9.50		m	31.2	198	1.022	0.075	553	37	-0.08	0.07	805.9	935.8
GI 125	10.15	1.49	dM1	15.4	510	0.015	0.007	7	4	-0.51	0.33	8.7	2.5
G246-026	11.72	1.50	M3	21.2	504	0.030	0.009	17	7	-0.36	0.27	19.5	10.5
BD+60 637	10.12	1.32	dK8	36.9	602	0.134	0.017	138	74	-0.18	0.12	98.7	160.8
GI 127 A	3.95	0.51	F7 IV	14.1	212	2.792	0.168	916	6	-0.09	0.06	2187.0	520.5
GI 127 B	6.70		G7 V	14.1	212	2.792	0.168	916	6	-0.09	0.06	2187.0	520.5
G078-028	12.39		m	15.2	498	0.014	0.007	8	48	-0.05	0.46	11.3	3.1
GI 135	7.03	0.66	G1.5 V	24.7	562	0.018	0.007	10	31	-1.00	0.32	5.5	4.0
GI 136	5.54	0.64	G2 V	12.1	328	0.095	0.020	35	15	-0.91	0.09	33.1	5.8
GI 137	4.82	0.68	G5 Ve	9.2	286	1.201	0.095	472	9	-0.36	0.07	768.9	77.1
GI 139	4.26	0.71	G5 V	6.1	519	0.026	0.009	10	13	-0.76	0.31	11.1	0.5
G077-046	11.37	1.50	M2	15.1	455	0.026	0.010	8	15	-1.00	0.45	7.9	2.1
G005-032	12.19	1.56	m	18.3	540	0.103	0.016	82	9	-0.20	0.14	74.4	29.7
GI 140 A	10.64	1.51	dM0	19.8	459	0.509	0.035	597	12	-0.15	0.07	382.8	179.6
GI 140 B	12.00			19.8	459	0.509	0.035	597	12	-0.15	0.07	382.8	179.6
GI 140.1A	8.47	1.13	K5 V	19.8	593	0.018	0.007	11	3			14.6	6.8
GI 140.1B	10.32	1.39	k	19.9	593	0.018	0.007	11	12			14.6	6.9
HD 21175	6.92		K0 V	17.1	394	0.422	0.036	356	7	-0.22	0.08	301.2	105.3
GI 141	7.86	1.16	K5 V	15.1	375	0.032	0.012	13	4	-0.21	0.39	22.9	6.2
LP 532-81	14.70		m+	23.0	508	0.025	0.009	15	3	-0.48	0.27	14.6	9.3
*GI 142	8.39	1.33	K7 V	12.6	2017	0.091	0.007	457	16	-0.49	0.07	52.0	9.9
LP 772-72	14.28		m	21.9	185	0.060	0.022	10	24	-0.45	0.35	35.4	20.3
LDS 3498?	14.37		m	21.9	185	0.060	0.022	10	32	-0.45	0.35	35.4	20.3
GJ 1060 A	14.00		DA5	17.4	96	0.067	0.031	10	71	0.21	0.47	62.9	22.7
GJ 1060 B	13.80		sdM3	17.4	96	0.067	0.031	10	67	0.21	0.47	62.9	22.7
GI 143.1	9.98	1.42	M0 V	21.6	590	0.021	0.008	10	5	-0.47	0.31	12.0	6.7
HD 21663 A	8.32	0.74	G5	46.3	426	0.018	0.008	7	34	-0.91	0.66	6.3	16.2
HD 21663 B	10.75	1.42	dK6	46.3	426	0.018	0.008	7	34	-0.91	0.66	6.3	16.2
Hy 207	10.79	1.39	K7 V	16.0	426	0.018	0.008	7	33	-0.91	0.66	6.3	1.9
GI 143.2A	4.71	0.39	F5 IV-V	21.4	356	0.071	0.017	32	16	-0.50	0.19	40.0	22.0
GI 143.2B	10.75	1.42	m	21.4	356	0.071	0.017	32	61	-0.50	0.19	40.0	22.0
GI 144	3.73	0.88	K2 V	3.2	374	2.822	0.233	327	7	-0.45	0.07	1672.0	20.7
GI 145	11.48	1.57	M3.5	10.9	412	0.030	0.011	8	17	-0.72	0.28	13.3	1.9
LP 54-19	14.17		m	22.5	555	0.076	0.013	64	5	-0.12	0.16	58.7	35.6
GI 146	8.60	1.31	K7 V	13.4	555	0.030	0.010	9	22	-0.78	0.19	12.3	2.6
Rob 233	13.86		dM5 :	13.9	369	0.051	0.015	20	22	-0.49	0.23	29.0	6.6
LP 413-18	12.74		g-k	23.3	381	0.141	0.021	91	31	-0.10	0.15	109.5	70.9
LP 413-19	13.29		g-k	23.3	381	0.141	0.021	91	13	-0.10	0.15	109.5	70.9
LTT 11203	12.79		dM3.1	16.9	390	0.070	0.016	27	8	-0.52	0.19	39.1	13.4
Wo 9119 A	9.07	1.06	dK5	50.0	402	0.160	0.021	127	14	-0.10	0.14	124.7	373.0
Wo 9119 B	12.87	1.49		50.0	402	0.160	0.021	127	6	-0.10	0.14	124.7	373.0
GI 150	3.53	0.92	K0 IVe	9.0	532	0.019	0.008	9	26	-0.66	0.29	9.2	0.9
Wo 9124	10.66	0.66	F8	123.5	382	0.127	0.021	81	74	0.62	0.14	147.6	2691.9
Wo 9125	10.81	0.70	G0	125.0	382	0.127	0.021	81	66	0.62	0.14	147.6	2759.6
Wo 9127	11.09	0.86	G3	101.0	382	0.127	0.021	81	83	0.62	0.14	147.6	1802.0
GI 152	6.99	0.88	K0 V	16.2	171	0.108	0.032	16	8	-0.73	0.16	47.8	15.1
GI 153 A	9.33	1.28	K7	17.4	542	0.049	0.011	36	41	-0.39	0.21	30.9	11.2
GI 153 B	11.30	1.54	M2.5	17.4	542	0.049	0.011	36	24	-0.39	0.21	30.9	11.2
GI 153 C	11.60			17.4	542	0.049	0.011	36	24	-0.39	0.21	30.9	11.2
GI 154	9.61	1.47	K7	14.6	367	0.036	0.012	17	9	-0.66	0.24	17.6	4.5
GI 155	4.22	0.42	F3 III	17.9	518	0.022	0.009	8	19	-1.00	0.14	6.7	2.6
Wo 9135	10.23	1.16	dK6	40.5	359	0.025	0.010	14	8	-0.06	0.39	20.1	39.5
HD 24496	6.81		G5	20.7	330	0.057	0.015	32	2	-0.39	0.26	35.6	18.2
Steph 430	11.22	1.53	M3	15.4	366	0.058	0.016	20	16	-0.50	0.21	32.8	9.3
HD 24409	6.54		G0	21.4	573	0.014	0.006	7	46	-0.90	0.33	4.8	2.7
GI 156.2	8.26	1.15	K4 V	16.0	480	0.026	0.010	12	16	-0.68	0.20	12.4	3.8
*GJ 1066	8.94	1.21	K4 V	17.6	576	0.069	0.011	37	9	-0.36	0.16	44.4	16.5
GI 157 A	8.04	1.11	K4 V	15.8	329	0.440	0.038	364	15	-0.36	0.08	281.4	83.8
GI 157 B	11.61	1.47	dM3 e	15.8	329	0.440	0.038	364	15	-0.36	0.08	281.4	83.8

Name	<i>V</i>	<i>B - V</i>	Sp. type	<i>d</i> (pc)	Exp.	<i>CR</i>	$\pm CR$	Li	Δ	<i>hr</i>	Δhr	f_{x-14}	L_{x27}
Gl 159	5.37	0.50	F6 V	19.2	320	1.524	0.100	774	10	-0.04	0.07	1234.1	546.1
Gl 160	5.90	0.62	G5 V	16.7	178	0.424	0.051	174	12	-0.27	0.12	291.6	97.6
Rob 256	12.89		dM5 e	16.3	327	0.155	0.024	103	23	-0.22	0.15	110.4	34.9
Gl 161.1	5.52	0.46	F7 V	21.3	473	0.843	0.044	999	9	-0.14	0.05	638.4	347.2
HD 26337	7.04		G2 IV-V	56.2	308	4.409	0.286	760	11	-0.15	0.06	3313.4	12511.7
G247-015	13.71	1.69	m	11.8	478	0.052	0.012	33	6	-0.52	0.18	29.0	4.8
HD 26018	8.19	0.84	G5	26.4	469	0.065	0.014	33	5	0.03	0.21	55.0	45.9
Gl 165.1	8.67	1.00	K3	27.9	523	0.049	0.012	31	11	-0.46	0.19	28.8	26.9
Gl 166 A	4.43	0.82	K1 Ve	5.0	341	0.179	0.025	93	46	-0.14	0.14	135.8	4.1
Gl 166 B	9.52	0.03	DA4	5.0	344	0.796	0.052	572	35	-0.29	0.06	539.4	16.4
Gl 166 C	11.17	1.67	dM4.5e	5.0	344	0.796	0.052	572	35	-0.29	0.06	539.4	16.4
G007-034	13.82		dM4 e	10.3	280	0.121	0.023	54	19	-0.35	0.17	77.8	9.9
Gl 167	7.64	1.13	K5 V	13.1	233	0.035	0.015	8	24	-1.00	9.99	10.6	2.2
Gl 167.1	4.25	0.30	F4 III	20.3	179	0.187	0.036	67	7	-0.10	0.19	145.3	71.5
Gl 167.3	4.44	1.07	K2 IV	18.2	1131	0.013	0.005	12	19	-1.00	0.32	3.8	1.5
LP 415-636	12.90	1.70	dM4.5e	22.6	462	0.108	0.017	77	23	-0.28	0.14	73.9	45.2
*GJ 2034	14.36	0.52	DA8+M		233	0.243	0.032	90	45	-0.06	0.11	194.0	
LDS 3584A	12.63		m	23.5	410	0.043	0.012	24	38	-0.27	0.26	29.2	19.4
LDS 3584B	14.97		m	23.5	410	0.043	0.012	24	35	-0.27	0.26	29.2	19.4
Wo 9155 A	6.88	0.66	G4 V	27.1	544	0.051	0.012	23	26	-0.89	0.20	18.5	16.2
Wo 9155 B	7.30		G6 V	27.1	544	0.051	0.012	23	17	-0.89	0.20	18.5	16.2
LHS 1668	14.10		M3.5	17.0	727	0.062	0.012	58	64	-0.07	0.17	49.5	17.1
G175-032	14.45		m	20.0	479	0.050	0.012	30	20	-0.12	0.22	38.1	18.2
Gl 169	8.27	1.35	K7 V	11.5	429	0.133	0.020	116	6	-0.37	0.13	84.6	13.3
Gl 170	13.91	1.73	M4.5	10.4	465	0.087	0.015	64	24	-0.30	0.16	58.3	7.6
LP 415-148	14.57	1.75	k-m	33.6	467	0.021	0.009	11	13	-0.02	0.41	17.6	23.7
HD 28495	7.74		G0	27.5	476	0.528	0.034	653	15	-0.18	0.06	388.8	353.0
G008-041	14.60		m	16.4	420	0.090	0.017	50	9	-0.16	0.18	67.2	21.6
Wo 9158	7.93	0.79	K1	26.8	551	0.026	0.009	12	86	0.56	0.34	29.3	25.2
GJ 1071	8.86	1.11	K5 V	22.5	596	0.046	0.011	28	35	-0.31	0.21	30.6	18.5
Gl 171.2A	8.42	1.12	dK5 ep	17.9	452	2.689	0.078	999	4	-0.05	0.03	2163.2	825.3
Gl 172	8.61	1.40	K8 Ve	10.2	512	0.079	0.014	63	5	-0.64	0.12	39.0	4.8
G039-029	12.53	1.65	m	9.8	452	0.310	0.028	324	5	-0.20	0.09	224.6	25.9
Steph 497	10.59	1.45	M1	15.1	509	1.594	0.155	275	8	-0.09	0.10	1248.6	341.9
Steph 502	11.24	1.47	M0	17.8	402	0.014	0.007	7	79	1.00	0.86	18.9	7.2
Wo 9163 AB	10.97	1.48	dM0	20.2	471	0.016	0.007	8	37	-1.00	0.51	4.9	2.4
Gl 174	8.00	1.10	K3 V	13.5	434	2.364	0.075	999	2	-0.21	0.03	1701.4	370.7
Gl 174.1A	4.44	0.34	F2 V	20.1	329	0.521	0.042	393	7	-0.33	0.08	341.6	165.4
Gl 174.1B	12.50			20.1	329	0.521	0.042	393	7	-0.33	0.08	341.6	165.4
Gl 176	9.98	1.52	dM2.5e	9.4	425	0.039	0.012	13	24	-0.18	0.28	28.6	3.0
Gl 176.1	5.05	0.38	F1 V	27.6	268	0.099	0.022	39	11	-0.16	0.20	73.7	67.3
Gl 176.3	7.59	0.89	K0 V	20.4	708	0.025	0.008	14	11	-0.79	0.18	10.5	5.3
Gl 177	5.49	0.63	G1 V	13.3	539	0.490	0.046	272	9	-0.34	0.09	319.0	67.7
Gl 178	3.19	0.45	F6 V	8.0	392	1.957	0.147	481	14	-0.23	0.07	1387.7	106.9
GJ 2035	8.77	1.01	K5 V	27.0	442	0.065	0.014	36	5	-0.09	0.22	50.8	44.1
GJ 2036 A	11.13	1.57	M2 Ve	11.2	600	1.084	0.108	170	20	-0.20	0.09	785.9	117.4
GJ 2036 B	12.15	1.60		11.2	600	1.084	0.108	170	20	-0.20	0.09	785.9	117.4
Wo 9169 A	7.02	0.55	F8	36.0	406	0.149	0.022	106	30	-0.27	0.14	102.8	159.1
Wo 9169 B	14.60		k	36.0	406	0.149	0.022	106	10	-0.27	0.14	102.8	159.1
GJ 2037	8.13	1.07	K3/4 V	18.0	503	0.013	0.006	7	8	-1.00	9.31	3.9	1.5
Gl 181	9.78	1.44	dM2 e	16.5	474	0.023	0.009	11	24	-0.84	0.16	8.9	2.9
Gl 182	10.09	1.39	dM0.5	26.7	393	0.651	0.042	667	14	-0.20	0.06	472.3	401.8
Gl 183	6.22	1.06	K3 V	8.8	387	0.032	0.012	9	13	-0.64	0.39	15.8	1.5
LP 476-207	11.47	1.52	dM3	32.1	420	0.661	0.060	340	6	-0.35	0.08	427.0	524.8
LHS 1723	12.10		m	6.4	387	0.104	0.019	50	5	-0.68	0.12	48.9	2.4
Gl 185 A	8.46	1.41	M0 V	8.5	426	0.025	0.012	8	14	-0.43	0.34	15.1	1.3
Gl 185 B	10.50			8.5	426	0.025	0.012	8	14	-0.43	0.34	15.1	1.3
G097-015	13.75		m	12.1	418	0.029	0.011	14	9	-0.33	0.30	19.2	3.4
Gl 187	5.37	0.43	F2 V	26.2	244	0.179	0.030	60	8	-0.23	0.16	126.9	104.1
Gl 187.2A	5.00	0.33	F0 V	26.2	450	0.051	0.013	22	19	-0.83	0.16	19.8	16.3
LP 716-35	12.97		M4 e	17.4	381	0.045	0.013	28	6	-0.36	0.24	28.7	10.4
HD 32850	7.75	0.80	K0 V	24.0	426	0.029	0.009	16	23	-0.22	0.33	20.6	14.2
Gl 189	4.71	0.52	F7 V	11.7	1236	0.484	0.110	26	14	-0.33	0.18	317.9	51.7
BD-21 1074	10.29	1.52	M2	11.6	395	1.147	0.099	382	6	-0.16	0.08	855.9	137.5
Steph 545	11.66	1.51	M3:	11.6	395	1.147	0.099	382	8	-0.16	0.08	855.9	137.5
G085-041	11.78	1.66	k	12.8	445	0.055	0.014	24	5	-0.58	0.22	28.9	5.7
GJ 1075	9.02	1.40	K7 V	11.5	1241	0.031	0.010	11	17	-0.90	0.20	10.9	1.7
Wo 9175	2.79	0.13	A3 III	27.2	408	0.176	0.024	115	17	-0.24	0.12	124.1	110.2
Gl 189.2	5.11	0.44	F2 V	25.0	406	0.021	0.009	8	50	-1.00	0.42	6.4	4.8
G085-044	12.48	1.50	M3	20.9	458	0.182	0.022	170	2	-0.13	0.12	139.0	72.5
Gl 190	10.30	1.50	M4	9.3	383	0.030	0.012	9	34	-1.00	0.28	9.1	0.9
Gl 191	8.85	1.55	M0 V	3.9	248	0.049	0.020	10	43	-0.75	0.15	21.1	0.4
Gl 194 A	0.71	0.80	G5 III	12.9	420	23.540	0.244	999	15	0.11	0.01	20934.1	4191.6
Gl 194 B	0.96		G0 III	12.9	420	23.540	0.244	999	15	0.11	0.01	20934.1	4191.6
Gl 195 A	10.20	1.50	dM2	13.2	425	0.137	0.020	91	18	-0.28	0.14	93.3	19.3
Gl 195 B	13.70		M4 :	13.2	425	0.137	0.020	91	18	-0.28	0.14	93.3	19.3
Gl 196	5.05	0.47	F6 V	21.0	519	0.020	0.007	11	10	-1.00	0.64	5.9	3.1
Gl 198	5.96	0.57	G0 V	24.9	417	0.028	0.010	14	48	-0.04	0.37	22.8	16.9
Gl 200 A	7.70	1.04	K3 V	16.9	412	0.030	0.010	11	57	-0.88	0.22	11.0	3.7
Gl 200 B	11.70		M2	16.9	412	0.030	0.010	11	57	-0.88	0.22	11.0	3.7

Name	<i>V</i>	<i>B</i> - <i>V</i>	Sp. type	<i>d</i> (pc)	Exp.	<i>CR</i>	$\pm CR$	Li	Δ	<i>hr</i>	Δhr	f_{x-14}	L_{x27}
Gl 199 A	9.33	1.27	K3/5 V	20.3	399	0.134	0.020	72	4	-0.36	0.13	85.7	42.2
Gl 199 B	13.50			20.3	399	0.134	0.020	72	4	-0.36	0.13	85.7	42.2
HD 34865	8.79	1.00	K3 V	24.3	431	0.023	0.009	10	8	-0.36	0.39	14.7	10.4
Gl 201	7.95	1.09	dK5 e	14.3	444	0.110	0.017	92	10	-0.49	0.13	62.8	15.4
Gl 202	4.99	0.53	F8 Ve	14.7	443	1.395	0.057	999	10	-0.13	0.04	1063.1	273.5
GJ 1079	7.74	0.94	K2/3 V	17.9	519	0.022	0.009	8	20	-0.58	0.28	11.6	4.4
G102-004	13.98	1.65	m	29.0	454	0.024	0.009	15	9	-0.35	0.30	15.2	15.3
Gl 204.1	6.99	0.77	G5 Ve	19.6	1150	0.106	0.017	71	18	-0.52	0.12	59.2	27.1
Gl 205	7.96	1.47	M1.5 V	5.7	455	0.196	0.022	152	11	-0.61	0.10	99.7	3.9
Gl 206	11.52	1.63	dM4 e	12.8	454	0.625	0.055	352	6	-0.34	0.08	407.1	79.4
GJ 1081	12.21	1.60	k-m	15.3	403	0.086	0.016	48	16	-0.25	0.18	60.1	16.9
Gl 207.1	11.53	1.57	dM2.5e	16.8	459	0.505	0.050	286	5	-0.18	0.10	371.8	125.6
G097-054	11.81	1.59	M3.5	12.4	453	0.022	0.009	10	32	-0.02	0.39	18.2	3.4
Gl 208	8.80	1.40	dM0	11.4	463	0.274	0.026	259	16	-0.46	0.09	160.7	24.9
Wo 9185	9.33	1.13	K5 V	32.5	1692	0.016	0.004	16	45	-0.32	0.26	10.6	13.3
Gl 209.1	5.30	0.46	F5 V	42.6	526	0.125	0.017	109	12	-0.14	0.14	94.3	204.3
Gl 211	6.23	0.84	K1 Ve	12.2	367	0.369	0.033	331	14	-0.55	0.08	199.0	35.7
GJ 1083 AB	14.85	1.88	m	10.4	435	0.043	0.012	22	28	0.01	0.25	35.8	4.6
Gl 212	9.75	1.48	M1	12.5	367	0.369	0.033	331	80	-0.55	0.08	199.0	37.1
G102-021	11.36	1.46	M3	28.8	462	0.319	0.028	350	9	-0.27	0.08	219.2	217.8
Wo 9188	10.61	1.46	dM0	21.5	448	0.017	0.008	9	6	0.58	0.52	19.7	10.9
Gl 213	11.53	1.62	M4	5.8	461	0.016	0.007	9	14	-0.61	0.39	8.2	0.3
Wo 9189	5.65	0.60	G1 V	18.2	1069	0.016	0.005	12	10	-0.72	0.21	7.0	2.8
Gl 216 B	6.13	0.94	K2 V	9.0	488	0.343	0.029	330	10	-0.52	0.06	190.5	18.3
Steph 578	10.99	1.45	M0	24.4	478	0.205	0.022	193	7	-0.28	0.11	140.2	100.3
GJ 1084	9.74	1.38	M0 V	20.7	916	0.037	0.008	47	8	-0.49	0.16	21.3	11.0
GJ 1085	5.97	0.64	G2 V	15.6	500	0.023	0.008	10	41	-0.78	0.23	9.5	2.7
Gl 222 AB	4.40	0.59	G0 V	8.7	431	1.942	0.068	999	9	-0.27	0.03	1335.9	120.0
Gl 224.1	4.65	1.05	K1 III/IV	27.2	3067	0.007	0.002	11	31	-1.00	0.73	2.1	1.9
Gl 225	3.72	0.33	F1 III	15.0	507	0.224	0.023	212	12	-0.37	0.09	142.0	38.4
G192-012	13.56		m	13.5	343	0.140	0.023	75	9	-0.34	0.15	91.0	19.8
G099-049	11.33	1.68	M4	5.4	475	0.404	0.045	193	7	-0.20	0.11	292.9	10.1
Gl 226	10.50	1.51	M2.5	9.4	534	0.019	0.008	7	20	-0.81	0.20	7.8	0.8
Wo 9200	6.35	0.52	G0 IV-V	26.7	933	0.636	0.028	889	77	-0.09	0.05	498.1	423.8
Gl 227	6.76	0.81	dK0 e	15.5	434	0.257	0.027	200	13	-0.39	0.10	160.8	45.9
Gl 229	8.14	1.50	M1 Ve	5.8	592	0.054	0.012	39	7	-0.38	0.18	33.7	1.3
Gl 230	6.45	0.67	G2 V	18.1	450	0.193	0.023	172	5	-0.37	0.10	122.6	48.1
HD 43162	6.38	0.72	G5 V	16.7	651	0.655	0.071	165	21	-0.39	0.10	408.7	136.3
Gl 231	5.08	0.72	G5 V	10.2	1166	0.017	0.005	21	16	-1.00	1.53	5.1	0.6
HD 43042	5.20	0.44	F6 V	21.1	403	0.140	0.020	95	8	-0.18	0.14	102.8	55.0
Wo 9207	5.04	0.42	F5 IV-V	19.6	454	0.352	0.029	380	1	-0.24	0.08	247.7	113.9
G101-035	12.27		m	23.3	299	0.265	0.033	156	7	-0.30	0.12	178.0	115.7
Gl 233 AB	6.76	0.94	K2 V e	14.7	394	1.741	0.069	999	6	-0.20	0.04	1262.2	324.7
Steph 598	11.09	1.50	M0	19.3	285	0.360	0.037	214	17	-0.32	0.10	238.2	106.6
LP 205-49	14.83		m	12.5	311	0.085	0.019	42	4	-0.22	0.21	60.7	11.4
Gl 239	9.63	1.49	dM1	9.8	447	0.025	0.009	15	13	-0.33	0.35	16.7	1.9
Gl 240	9.62	1.46	K0	15.1	948	0.041	0.009	39	3	-0.61	0.14	20.7	5.7
HD 48189 A	6.34	0.62	G0 V	21.6	966	2.325	0.050	999	6	-0.15	0.02	1747.2	979.4
HD 48189 B	8.30			21.6	966	2.325	0.050	999	6	-0.15	0.02	1747.2	979.4
Gl 240.1	5.45	0.50	F8 V	17.9	528	0.017	0.007	9	20	-1.00	0.89	5.0	1.9
Gl 241	8.13	1.02	dK6	17.5	439	0.023	0.010	7	9	-0.04	0.37	18.9	7.0
Wo 9216	10.95	1.48	K7	22.5	411	0.021	0.009	10	5	-1.00	0.38	6.4	3.9
G192-039	12.44	1.59	M3.5	19.1	298	0.051	0.016	14	15	-0.41	0.30	31.1	13.6
G192-039	14.90			19.1	298	0.051	0.016	14	15	-0.41	0.30	31.1	13.6
Gl 242	3.36	0.43	F5 III	17.5	451	0.393	0.031	443	6	-0.04	0.08	318.6	117.3
Gl 244 A	-1.43		A1 V	2.6	272	12.730	0.219	999	8	-1.00	0.00	3831.7	31.9
Gl 244 B	8.44	-0.03	DA2	2.6	272	12.730	0.219	999	8	-1.00	0.00	3831.7	31.9
Gl 245	5.24	0.56	G0 V	16.5	337	0.048	0.014	17	43	-0.19	0.30	34.8	11.3
Gl 245.1	5.92	0.49	F6 V	24.3	577	0.015	0.006	9	24	-0.65	0.32	7.1	5.0
Gl 248	3.27	0.21	A7 IV	30.3	1213	0.078	0.009	138	6	-0.13	0.12	59.2	65.1
Gl 249.1	5.13	0.45	F5 III	25.2	606	0.016	0.006	10	30	-0.88	0.32	5.8	4.4
Gl 250 A	6.59	1.05	K3 V	8.7	269	0.229	0.032	152	7	-0.51	0.12	128.6	11.7
Gl 250 B	10.09	1.50	M2	8.7	269	0.229	0.032	152	66	-0.51	0.12	128.6	11.7
Wo 9220 A	4.74	0.31	A9 V p	27.9	344	0.263	0.031	196	5	-0.22	0.11	188.2	175.7
Wo 9220 B	7.68	0.72	G6 V	27.9	344	0.263	0.031	196	5	-0.22	0.11	188.2	175.7
G250-031	13.65		m	11.4	350	0.331	0.033	242	8	0.01	0.10	277.2	43.4
Wo 9222	7.65	0.53	F8 V +A/F	53.8	804	0.018	0.006	17	25			15.0	52.0
Gl 255 A	6.91	0.46	F8 IV-V	43.3	432	0.412	0.032	462	6	-0.02	0.08	338.0	757.9
Gl 255 B	7.10		F8 IV-V	43.3	432	0.412	0.032	462	6	-0.02	0.08	338.0	757.9
Gl 256	9.15	1.16	K4 V	22.3	445	0.503	0.034	661	6	-0.24	0.07	354.2	211.2
Gl 259	6.71	0.89	K0 Ve	14.6	443	0.198	0.024	154	4	-0.42	0.10	120.8	30.9
Gl 260	6.82	0.80	K0 IV-V	18.4	1481	0.192	0.012	557	8	-0.38	0.06	120.7	49.0
GJ 1094	8.38	1.08	K5 V	18.7	416	0.022	0.009	8	35	-0.52	0.34	12.2	5.1
Gl 268	11.49	1.71	M4.5 Ve	6.4	202	0.257	0.041	79	20	-0.56	0.12	137.3	6.6
Gl 268.1	4.48	0.32	F0 IV	21.2	176	0.106	0.027	34	22	-0.58	0.19	55.6	29.9
Gl 268.2	9.10	1.25	K5 V	20.0	1217	0.013	0.005	10	17	-0.65	0.22	6.4	3.1
GJ 1096	14.48	1.75	m+	14.9	437	0.081	0.015	56	15	-0.39	0.17	50.4	13.5
Gl 268.3	10.85	1.54	dM0	12.3	402	0.020	0.009	9	83	-1.00	0.46	6.1	1.1
Gl 269 A	7.15	0.99	K1 V	14.8	175	0.251	0.041	101	6	-0.06	0.16	200.7	52.4
Gl 269 B	7.90		K4 V	14.8	175	0.251	0.041	101	6	-0.06	0.16	200.7	52.4

Name	V	$B - V$	Sp. type	$d(\text{pc})$	Exp.	CR	$\pm CR$	Li	Δ	hr	Δhr	f_{x-14}	L_{x27}
GI 271 A	3.53	0.34	F1 IV-V	18.0	443	0.108	0.019	57	18	-0.57	0.13	57.2	22.2
GI 271 B	8.20		K3 V	18.0	443	0.108	0.019	57	18	-0.57	0.13	57.2	22.2
GI 272	10.53	1.46	dM2	16.2	412	0.015	0.007	11	15	-0.35	0.40	9.7	3.1
LHS 1909	11.75		m	22.4	388	0.028	0.010	18	39	-0.31	0.31	18.4	11.1
GI 273	9.85	1.56	M3.5	3.8	247	0.034	0.015	9	39	-1.00	0.74	10.2	0.2
GI 273.1	7.74	0.94	dK8	17.5	441	0.055	0.013	31	19	-0.62	0.18	27.7	10.2
GI 274 A	4.18	0.32	F0 V	18.5	445	0.347	0.029	399	1	-0.29	0.08	234.9	96.0
GI 274 B	12.50			18.5	445	0.347	0.029	399	1	-0.29	0.08	234.9	96.0
GI 277 A	10.58	1.47	dM3.5e	11.4	455	1.006	0.048	999	30	-0.21	0.05	724.0	112.9
GI 277 B	11.78	1.52	dM4.5e	11.5	455	1.006	0.048	999	8	-0.21	0.05	724.0	113.9
HD 59967	6.64	0.63	G4 V	21.8	271	0.320	0.037	195	13	-0.36	0.10	205.1	116.5
GI 278 A	1.94	0.04	A1 V	15.8	440	3.697	0.091	999	58	-0.16	0.03	2758.7	823.7
GI 278 B	2.85		A m	15.8	440	3.697	0.091	999	58	-0.16	0.03	2758.7	823.7
GI 278 C	9.07	1.49	M0.5Ve	15.8	440	3.697	0.091	999	16	-0.16	0.03	2758.7	823.7
GI 280 A	0.38	0.42	F5 IV-V	3.5	400	3.655	0.098	999	8	-0.90	0.01	1293.9	18.9
GI 280 B	10.70		DA	3.5	400	3.655	0.098	999	8	-0.90	0.01	1293.9	18.9
GI 282 A	7.20	0.96	K2 Ve	14.2	128	0.128	0.038	18	13	-0.67	0.20	60.9	14.7
GI 282 B	8.94	1.33	K5	14.2	128	0.128	0.038	18	49	-0.67	0.20	60.9	14.7
GI 285	11.20	1.60	dM4.5e	5.9	253	1.467	0.079	999	30	-0.21	0.05	1055.8	44.4
GI 285.1	7.09	0.66	dG5	28.5	307	0.089	0.019	41	3	-0.65	0.24	43.2	42.0
GI 286	1.14	1.00	K0 IIIb	10.3	411	0.059	0.014	23	12	-0.75	0.19	25.7	3.3
GJ 1101	13.09	1.68	m	12.5	680	0.183	0.018	239	3	-0.22	0.09	130.4	24.2
GI 290	6.56	0.73	G8 V	17.0	551	0.021	0.008	9	23	-0.67	0.26	9.8	3.4
GI 292 A	5.05	0.44	F5 V	18.0	154	0.589	0.063	226	9	-0.20	0.11	426.9	165.8
GI 292 B	8.60		K3	18.0	154	0.589	0.063	226	9	-0.20	0.11	426.9	165.8
LHS 1955	13.38		M4	12.6	243	0.037	0.016	8	45	-0.35	0.35	23.8	4.5
GI 293.1A	8.06	1.04	K5 V	17.5	366	0.024	0.010	8	23	-0.58	0.32	12.5	4.5
GI 293.1B	13.30			17.5	366	0.024	0.010	8	23	-0.58	0.32	12.5	4.5
GI 293.2	8.42	1.05	K3 V	18.2	221	0.036	0.015	13	21	-0.75	0.27	15.8	6.3
Wo 9247	7.95	0.74	G6 V	29.3	220	0.029	0.014	8	22	-0.88	0.81	10.5	10.8
HD 67199	7.14	0.94	K1 V	17.3	929	0.036	0.008	31	35	-0.48	0.16	20.8	7.4
BD+26 1715	10.21	1.46	M0	17.9	403	0.021	0.009	9	9	-0.74	0.24	9.0	3.4
G040-007	9.80	1.38	K5	17.1	212	0.767	0.064	458	15	-0.31	0.08	511.4	179.4
LHS 5134	11.00		m	17.1	212	0.767	0.064	458	16	-0.31	0.08	511.4	179.4
GJ 1108 A	10.05	1.35	dM0.5e	20.7	274	0.777	0.056	504	12	-0.29	0.07	526.4	270.0
GJ 1108 B	12.12	1.53	dM3 e	20.7	274	0.777	0.056	504	3	-0.29	0.07	526.4	270.0
GI 297.1	4.76	0.43	F5 V	21.4	366	0.351	0.032	292	5	-0.19	0.09	256.6	140.2
GI 302	5.97	0.76	G7.5 V	12.6	355	0.032	0.011	13	6	-0.65	0.29	15.7	3.0
GI 305	4.07	0.40	F6 IV	19.5	560	0.229	0.022	257	6	-0.13	0.09	174.9	79.2
GI 306	5.61	0.46	F3 V	27.2	307	0.686	0.050	548	16	0.01	0.07	574.0	507.1
GJ 2069 A	11.89		M5 e	12.8	314	0.726	0.050	580	5	-0.14	0.07	549.5	107.8
GJ 2069 B	13.32			12.8	314	0.726	0.050	580	17	-0.14	0.07	549.5	107.8
LHS 2024	15.00		m	16.5	245	0.016	0.010	9	63			13.4	4.4
G234-037	11.67	1.57	M3	12.9	430	0.037	0.011	15	25	-1.00	0.41	11.1	2.2
HD 72760	7.32		G5	21.7	294	0.096	0.022	39	8	-0.34	0.19	62.8	35.5
GI 310.1A	5.99	0.52	F8 V	26.5	333	0.118	0.021	49	8	-0.52	0.14	65.8	55.4
GI 310.1B	7.25	0.71	G5 IV-V	23.4	333	0.118	0.021	49	14	-0.52	0.14	65.8	43.2
GI 311	5.64	0.62	G1 V	14.3	392	0.797	0.047	820	6	-0.32	0.06	526.9	128.3
Wo 9273	6.75	0.66	G0	23.6	282	0.130	0.024	57	4	-0.26	0.17	90.2	60.3
GI 314 A	5.28	0.73	G3 V	19.9	374	0.047	0.014	17	22	-0.76	0.21	20.1	9.6
GI 314 B	6.80		K0 V	19.9	374	0.047	0.014	17	22	-0.76	0.21	20.1	9.6
GI 316.1	17.68	2.02	m	14.1	170	0.417	0.054	127	20	-0.07	0.13	331.1	78.4
GI 320	6.56	0.93	K1 V	11.1	505	0.460	0.047	216	14	-0.31	0.10	306.9	45.5
GI 321.3A	2.02	0.04	A0 V	24.4	553	0.264	0.034	109	11	-0.24	0.13	185.9	133.0
GI 321.3B	5.00			24.4	553	0.264	0.034	109	11	-0.24	0.13	185.9	133.0
GI 321.3C	11.00			24.4	553	0.264	0.034	109	60	-0.24	0.13	185.9	133.0
GI 321.3D	13.50			24.4	553	0.264	0.034	109	60	-0.24	0.13	185.9	133.0
GI 322	9.28	1.34	dM0	16.5	421	0.075	0.016	32	26	-0.23	0.19	53.0	17.3
GI 323 A	9.77	1.36	dM0 p	17.0	246	0.097	0.024	26	17	0.04	0.24	82.9	28.6
GI 323 B	9.90			17.0	246	0.097	0.024	26	17	0.04	0.24	82.9	28.6
GI 325 A	8.70	1.39	K5 V	11.4	423	0.059	0.014	25	19	-1.00	0.11	17.8	2.8
GI 325 B	8.90		K6 V	11.4	423	0.059	0.014	25	18	-1.00	0.11	17.8	2.8
GI 327	6.00	0.67	G3 V	17.1	307	0.118	0.023	49	11	-0.58	0.14	61.8	21.6
GI 329	8.66	1.00	K2/3 III	31.2	232	0.030	0.013	9	37			24.8	28.8
LHS 2071	14.00		m	12.7	242	0.036	0.015	10	26	-0.27	0.37	24.5	4.8
HD 76653	5.71	0.48	F6 V	24.2	440	0.461	0.034	403	2	-0.31	0.07	307.0	214.3
G252-025	14.32	1.70	m	13.8	423	0.018	0.008	8	65	0.34	0.46	18.6	4.2
GJ 1116 A	14.06	1.84	m	5.2	337	0.340	0.034	231	66	-0.17	0.10	251.9	8.2
GJ 1116 B	14.92	1.93	m	5.2	337	0.340	0.034	231	60	-0.17	0.10	251.9	8.2
GI 331 A	3.14	0.19	A7 IV	14.6	285	0.169	0.027	81	6	-0.35	0.14	109.3	28.0
GI 331 B	10.80		dM1	14.6	285	0.169	0.027	81	6	-0.35	0.14	109.3	28.0
GI 331 C	11.00			14.6	285	0.169	0.027	81	6	-0.35	0.14	109.3	28.0
G041-014	10.89	1.67	k	6.5	351	1.526	0.119	441	8	-0.13	0.08	1163.0	58.1
GJ 1119	13.32	1.72	m	10.3	308	0.031	0.013	10	26	-0.15	0.37	23.2	3.0
GI 332 A	4.11	0.37	F3 V	16.4	400	0.676	0.045	543	6	-0.46	0.06	396.9	128.1
GI 332 B	6.18	0.65	G5 V	16.4	400	0.676	0.045	543	6	-0.46	0.06	396.9	128.1
HD 77137	6.87	0.69	G5 V	55.9	424	1.604	0.127	492	11	0.15	0.08	1460.4	5453.4
GI 333.1	5.16	0.42	F3 V	26.2	355	0.219	0.028	155	8	-0.32	0.11	144.6	118.6
GI 334	9.51	1.42	dM0	14.5	362	0.073	0.017	36	5	-0.26	0.21	50.5	12.7
GI 334.2	5.93	0.60	F9 V	19.1	411	0.334	0.030	284	8	-0.42	0.08	203.1	88.9

Name	V	$B - V$	Sp. type	$d(\text{pc})$	Exp.	CR	$\pm CR$	Li	Δ	hr	Δhr	f_{x-14}	L_{x27}
W _o 9286	5.99	0.65	G5 IV	31.2	365	0.090	0.018	39	43	-0.65	0.14	43.7	51.1
Gl 335 A	4.84	0.49	F7 IV-V	20.4	438	0.059	0.014	23	24	-0.79	0.16	24.2	12.1
Gl 335 B	8.44		K2 V	20.4	438	0.059	0.014	23	24	-0.79	0.16	24.2	12.1
W _o 9287 A	6.77	0.57	G1 V	44.6	439	0.028	0.010	10	85	-0.61	0.35	14.4	34.4
W _o 9287 B	13.00			44.6	439	0.028	0.010	10	85	-0.61	0.35	14.4	34.4
09 07 00 +06 54.	13.35	1.57	M4 e	20.8	373	0.127	0.020	73	28	-0.51	0.13	71.4	37.1
HD 78727	8.38	1.01	K4	21.5	369	0.045	0.015	15	17	-0.06	0.31	36.0	19.9
HD 78899	7.68		G5	36.8	484	0.239	0.024	224	25	-0.25	0.09	166.9	270.0
Gl 337 A	7.25	0.73	K0 V	20.5	189	0.061	0.022	14	19	-1.00	0.45	18.5	9.3
Gl 337 B	7.30			20.5	189	0.061	0.022	14	19	-1.00	0.45	18.5	9.3
Gl 338 A	7.62	1.39	M0 Ve	6.2	326	0.257	0.030	149	3	-0.67	0.09	122.3	5.6
Gl 338 B	7.71	1.42	M0 Ve	6.1	326	0.257	0.030	149	17	-0.67	0.09	122.3	5.5
Gl 338.1A	10.67	1.38	K5	27.2	470	0.020	0.008	9	33	-0.27	0.36	13.4	11.9
Gl 338.1B	11.00			27.2	470	0.020	0.008	9	33	-0.27	0.36	13.4	11.9
Gl 339 AB	8.04	1.02	dK5	18.4	368	0.423	0.037	373	5	-0.36	0.08	270.9	109.9
Gl 339.3	4.62	0.45	F5 III	50.8	572	0.038	0.011	9	51	-0.56	0.30	20.1	62.1
LTT 3412	10.75	1.55	M2	12.7	352	0.044	0.013	27	31	-0.35	0.25	28.4	5.5
HD 79873	6.71	0.41	F6 III-IV	69.0	338	0.126	0.021	56	15	-0.14	0.16	95.2	541.8
Gl 340 A	7.86	1.00	K3 V	17.5	340	0.041	0.014	11	36	-0.74	0.27	18.2	6.7
Gl 340 B	8.10		K3 V	17.5	340	0.041	0.014	11	36	-0.74	0.27	18.2	6.7
BD+27 1739	9.55	1.34	K5	19.3	364	0.027	0.011	10	15	-0.19	0.35	19.7	8.8
G235-020	11.28		m	32.5	350	0.200	0.026	149	10	-0.16	0.13	149.2	188.1
GJ 1122 A	14.52	1.68	m	20.2	459	0.034	0.012	14	8	-0.61	0.20	17.5	8.6
GJ 1122 B	14.67	1.68	m	20.2	459	0.034	0.012	14	14	-0.61	0.20	17.5	8.6
Gl 340.1A	6.13	0.42	F4 V	33.6	297	0.049	0.015	19	9	-0.32	0.27	32.2	43.4
Gl 340.1B	6.13			33.6	297	0.049	0.015	19	9	-0.32	0.27	32.2	43.4
G115-071	14.02		m	15.4	468	0.032	0.011	19	7	0.08	0.33	28.3	8.0
GJ 1124	7.63	0.99	K2 V	24.3	450	2.908	0.082	999	8	-0.02	0.03	2385.7	1681.6
Gl 342	9.03	1.19	dK5 e	20.1	497	0.040	0.011	17	10	-1.00	0.15	12.0	5.8
Gl 343.1	9.84	1.29	dK8 e	32.3	430	0.100	0.017	52	14	-0.30	0.16	67.2	83.7
Gl 344 A	5.80	0.65	G2 V	31.2	395	0.030	0.012	9	22	-0.89	0.27	10.7	12.6
Gl 344 B	6.60			31.2	395	0.030	0.012	9	22	-0.89	0.27	10.7	12.6
Gl 346	10.52	1.43	dM0	20.5	364	0.044	0.014	17	13	-0.03	0.30	35.9	18.1
Gl 348 A	4.60	0.45	F6 V	17.1	365	0.574	0.041	507	18	-0.26	0.07	398.0	139.1
Gl 348 B	7.18	0.87	K0	17.1	365	0.574	0.041	507	48	-0.26	0.07	398.0	139.1
Gl 349	7.20	1.00	K3 Ve	12.7	385	0.184	0.023	136	4	-0.51	0.11	103.3	19.9
HD 81937	3.67	0.33	F0 IV	23.1	346	0.042	0.013	14	9	-1.00	0.45	12.7	8.2
Gl 351 A	4.12	0.36	F3 IV	18.6	427	0.558	0.038	552	6	-0.34	0.06	363.3	149.6
Gl 351 B	4.65		F0 IV	18.6	427	0.558	0.038	552	6	-0.34	0.06	363.3	149.6
Gl 352 A	10.81	1.53	M3	10.5	402	0.018	0.009	8	10	-0.43	0.32	10.7	1.4
Gl 352 B	10.80			10.5	402	0.018	0.009	8	10	-0.43	0.32	10.7	1.4
Gl 354.1A	7.01	0.77	dG9	17.8	434	0.731	0.043	770	5	-0.20	0.06	530.3	200.2
Gl 354.1B	16.50		m	17.8	434	0.731	0.043	770	57	-0.20	0.06	530.3	200.2
Gl 355	7.82	0.92	K0	18.3	445	2.730	0.202	583	10	-0.04	0.07	2210.8	890.5
Gl 355.1	4.56	0.77	G4 III-IV	32.4	419	2.029	0.071	999	3	0.05	0.03	1739.9	2180.2
Gl 356 A	5.41	0.77	G8 V	11.2	467	0.298	0.027	254	27	-0.55	0.08	160.9	24.1
Gl 356 B	13.00			11.2	467	0.298	0.027	254	27	-0.55	0.08	160.9	24.1
W _o 9303	11.02	1.44	K5	33.2	431	0.075	0.017	22	27	-0.18	0.20	55.1	72.8
Gl 358	10.75	1.53	M3	9.5	410	0.175	0.023	118	17	-0.31	0.13	116.8	12.6
Gl 360	10.57	1.50	M3	11.8	299	0.179	0.029	70	68	-0.40	0.13	110.7	18.3
Gl 361	10.37	1.50	dM2 e	11.4	409	0.038	0.012	16	9	-0.42	0.28	23.2	3.6
Gl 362	11.22	1.52	M3	11.5	299	0.179	0.029	70	33	-0.40	0.13	110.7	17.6
Gl 365	8.12	1.15	K5 V	17.8	413	0.035	0.013	10	18	-0.67	0.24	16.5	6.2
G042-024	14.05		m	10.3	361	0.023	0.010	8	11	-0.51	0.32	13.2	1.7
Gl 373	9.00	1.43	dM1	10.5	596	0.059	0.012	44	8	-0.52	0.17	32.7	4.3
G116-065	12.73		M4	19.0	445	0.105	0.019	57	25	-0.41	0.14	64.2	27.7
HD 86146	5.14	0.46	F6 Vas	28.9	366	0.087	0.019	31	9	-0.67	0.15	41.5	41.5
G116-072	13.89		m	22.6	484	0.216	0.024	149	5	-0.26	0.10	150.0	91.9
G116-073	14.16		m	22.6	484	0.216	0.024	149	21	-0.26	0.10	150.0	91.9
Gl 375	11.27	1.55	M3.5	15.9	394	0.805	0.067	431	3	-0.17	0.08	596.5	180.4
HD 86590	7.90	0.88	K0 V	32.5	452	2.053	0.068	999	12	-0.02	0.03	1684.3	2124.2
Gl 378.1	9.04	1.07	dK8	27.7	507	0.055	0.014	21	14	-0.63	0.16	27.5	25.2
Gl 378.2	9.95	1.39	dM0 e	22.3	435	0.023	0.009	9	22	-0.32	0.35	15.3	9.1
Gl 380	6.59	1.36	K2 Ve	4.9	494	0.177	0.021	153	9	-0.54	0.09	96.3	2.7
Gl 382	9.27	1.48	dM2	7.8	430	0.065	0.015	32	2	-0.67	0.19	30.9	2.3
Gl 384 A	8.27	0.80	G8 V	41.0	354	0.047	0.014	18	10	-0.04	0.28	38.3	77.0
Gl 384 B	10.90			41.0	354	0.047	0.014	18	10	-0.04	0.28	38.3	77.0
Gl 385.1	6.38	0.59	G1 V	22.7	281	0.080	0.021	23	35	-0.14	0.24	60.8	37.6
W _o 9321	7.21	0.49	dF6	48.3	379	0.134	0.020	94	4	0.00	0.16	111.4	311.2
GJ 2079	10.20	1.36	dM0 e	20.4	300	0.507	0.043	353	11	-0.38	0.08	319.5	159.2
Gl 388	9.40	1.54	M4.5Ve	4.9	104	3.701	0.194	999	7	-0.28	0.05	2526.3	72.2
Gl 388.2	7.18	0.55	F8 V	34.6	398	0.035	0.011	17	4	-0.82	0.18	13.9	19.9
Gl 390	10.17	1.49	M1.5	12.5	401	0.016	0.007	9	9	-0.71	0.54	7.3	1.4
*Gl 391	4.00	0.35	F2 IV	16.2	606	0.100	0.013	148	42	-0.44:	0.21:	59.9:	18.8:
Gl 392.1	5.26	0.37	F2 V	21.5	329	0.309	0.033	181	6	-0.21	0.11	222.5	123.1
G118-061	13.00		m	19.1	463	0.019	0.009	7	8	-0.50	0.31	11.0	4.8
Gl 393	9.64	1.52	dM2.5	7.2	401	0.025	0.011	10	10	-0.73	0.21	11.2	0.7
Gl 395	4.84	0.52	F8 V	12.9	572	0.195	0.021	172	5	-0.68	0.07	92.0	18.2
Gl 396	7.30	0.82	K0	21.1	589	0.032	0.009	18	12	-0.64	0.20	15.9	8.4
Gl 397	8.86	1.33	K7 V	15.7	392	0.060	0.015	20	18	-0.36	0.23	38.3	11.3

Name	V	$B - V$	Sp. type	$d(\text{pc})$	Exp.	CR	$\pm CR$	Li	Δ	hr	Δhr	f_{x-14}	L_{x27}
GI 397.1A	9.65	1.38	dM0 e	17.5	543	0.038	0.010	25	6	-0.75	0.16	16.6	6.1
BD-20 3198	10.68	1.38	K7 V	29.2	256	0.149	0.027	58	16	-0.19	0.18	109.1	111.0
DON 414C	13.13	1.57		29.2	256	0.149	0.027	58	16	-0.19	0.18	109.1	111.0
GI 398	12.60	1.60	dM4 e	14.5	165	0.205	0.039	48	39	-0.26	0.19	142.2	36.0
LP 167-71	13.49		m	22.4	542	0.068	0.014	39	5	-0.58	0.15	35.8	21.4
GJ 1136 A	10.19	1.46	K7 V	16.3	297	0.048	0.016	11	24	-0.87	0.16	17.9	5.7
GJ 1136 B	11.67	1.52		16.3	297	0.048	0.016	11	24	-0.87	0.16	17.9	5.7
HD 92945	7.74	0.89	K1 V	21.6	361	0.118	0.020	68	9	-0.13	0.17	89.6	49.8
GI 400 A	9.30	1.41	dM2	14.1	455	0.022	0.009	8	4	-1.00	0.35	6.5	1.6
GI 400 B	12.20			14.1	455	0.022	0.009	8	4	-1.00	0.35	6.5	1.6
HD 93811	8.33		G5	28.7	548	0.157	0.020	110	11	-0.22	0.11	112.0	110.7
LP 263-35	13.46		m	24.5	327	0.127	0.022	73	6	-0.03	0.17	103.4	74.3
G045-011	13.85		m	15.9	415	0.186	0.024	138	9	-0.09	0.13	146.1	44.0
G044-043	14.40		m	19.0	333	0.071	0.017	33	17	-0.26	0.21	48.9	21.1
Wo 9336	7.05	0.64	G3/5 V	41.3	345	0.145	0.024	94	0	0.02	0.16	121.6	248.4
GI 403.1	5.23	0.46	F6 V	31.3	289	0.070	0.018	37	15	0.14	0.24	63.7	74.9
GI 404.1	3.78	0.95	K1 III	29.7	192	0.135	0.029	45	4	-0.05	0.21	108.5	114.3
HD 94765	7.34	0.92	K0	17.5	344	0.153	0.022	87	5	-0.36	0.15	98.2	36.2
GI 406	13.45	2.00	M6	2.4	384	0.227	0.026	183	18	-0.22	0.11	162.5	1.1
G147-011	15.36	1.75	m	22.3	352	0.020	0.010	8	13	-0.52	0.35	11.4	6.8
GI 408	10.02	1.54	M3	6.6	212	0.026	0.013	8	39	-1.00	1.51	8.0	0.4
GI 410	9.60	1.48	dM2 e	11.7	178	0.240	0.039	87	9	-0.42	0.16	146.3	23.8
LP 263-64	13.67		m	21.1	360	0.108	0.020	53	7	-0.30	0.17	72.8	38.8
GI 411	7.48	1.51	M2 Ve	2.5	341	0.167	0.024	83	10	-0.67	0.10	79.5	0.6
HD 96202	5.63	0.37	F3 IV	43.5	289	0.032	0.013	12	8	-1.00	0.26	9.6	21.6
GI 412 A	8.74	1.54	M2 Ve	4.8	364	0.185	0.027	111	25	-0.65	0.09	89.9	2.5
GI 412 B	14.40	2.09	M6 e	4.8	364	0.185	0.027	111	13	-0.65	0.09	89.9	2.5
GI 414 A	8.33	1.34	K8 V	11.9	317	0.046	0.016	10	36	-0.80	0.18	18.7	3.2
GI 414 B	9.98	1.52	M2 V	11.9	317	0.046	0.016	10	36	-0.80	0.18	18.7	3.2
G119-062	12.38		dM4	14.6	262	0.366	0.040	201	4	-0.21	0.11	263.3	67.5
GI 416.1	4.48	0.03	A2 III	81.3	293	0.469	0.043	206	11	-1.00	0.04	141.1	1116.2
GI 417	6.41	0.61	G0 V	21.7	207	0.320	0.045	114	11	-0.26	0.13	222.0	125.5
GI 418	8.69	1.18	K5 V	18.0	422	0.036	0.011	17	8	-0.91	0.22	12.6	4.9
GI 420 A	7.68	1.06	dK5	14.7	483	0.117	0.018	66	14	-0.40	0.13	72.5	18.7
GI 420 B	11.40		M2	14.7	483	0.117	0.018	66	14	-0.40	0.13	72.5	18.7
Steph 932	11.22	1.41	M0	23.8	547	0.323	0.027	337	7	-0.25	0.08	225.7	152.3
GI 421.1A	6.50	0.43	F6 V	39.2	384	0.034	0.012	11	85	-0.69	0.32	15.7	28.9
GI 421.1B	8.03	0.60	F9 V	45.2	384	0.034	0.012	11	87	-0.69	0.32	15.7	38.4
GI 423 A	4.33	0.59	G0 Ve	8.8	192	4.539	0.157	999	7	-0.21	0.03	3266.7	305.0
GI 423 B	4.80		G0 Ve	8.8	192	4.539	0.157	999	7	-0.21	0.03	3266.7	305.0
GI 424	9.31	1.41	M1 V	9.1	619	0.018	0.007	9	17	-0.63	0.30	9.0	0.9
GI 425 A	8.74	1.36	K4/5 V	13.2	292	0.914	0.057	716	11	-0.13	0.06	696.3	144.2
GI 425 B	11.00		m	13.2	292	0.914	0.057	716	11	-0.13	0.06	696.3	144.2
GJ 2084 AB	9.08	1.26	K4 V	46.7	330	0.656	0.046	529	9	0.06	0.07	566.3	1479.6
G253-050	12.15		M2.5	18.4	520	0.021	0.008	8	67	-1.00	0.25	6.3	2.5
G253-049	12.65		M3	27.2	520	0.021	0.008	8	27	-1.00	0.25	6.3	5.6
GI 428 A	7.50	1.26	K7 V	12.9	209	0.076	0.022	25	13	-0.43	0.27	45.7	9.1
GI 428 B	8.30		M0 Ve	12.9	209	0.076	0.022	25	13	-0.43	0.27	45.7	9.1
GI 429 A	6.50	0.80	K0 IV	17.7	386	0.030	0.012	7	39	-0.99	0.21	9.2	3.4
GI 429 B	7.58	1.00	K2 IV-V	18.0	386	0.030	0.012	7	64	-0.99	0.21	9.2	3.6
GI 429.4	8.33	1.06	K4 Ve	22.2	137	0.076	0.027	11	19	-0.52	0.35	42.3	25.0
HD 100180	6.20	0.57	G0 V	23.0	398	0.031	0.010	16	13	-1.00	1.22	9.2	5.9
LTT 13146	9.22	1.14	K6 IV	23.0	398	0.031	0.010	16	13	-1.00	1.22	9.2	5.9
GI 431	11.52	1.54	M3.5	10.5	210	0.662	0.060	440	8	-0.38	0.08	417.0	54.7
Wo 9367	5.77	0.46	F6 V	26.5	417	0.242	0.027	197	7	-0.33	0.10	158.7	133.6
G122-036	10.03	1.35	K5	24.4	248	0.028	0.013	9	6	-0.98	0.79	8.8	6.3
HD 101206	8.26	0.96	K5 V	19.8	255	0.107	0.024	30	22	0.32	0.22	107.1	50.0
GI 434	5.33	0.72	G8 Ve	9.5	314	0.348	0.037	194	15	-0.76	0.07	149.0	16.2
GI 436	10.67	1.52	dM3.5	10.2	455	0.018	0.008	7	58	-1.00	2.26	5.4	0.7
GI 441	9.02	1.17	dK8	27.5	759	0.022	0.007	17	10	-0.49	0.25	12.7	11.6
G236-081	13.60		m	16.5	805	0.094	0.013	88	12	-0.23	0.13	66.4	21.7
G010-049	13.25		m	14.6	373	0.114	0.020	75	11	-0.24	0.16	80.1	20.5
LP 613-50	17.60		m	14.6	373	0.114	0.020	75	22	-0.24	0.16	80.1	20.5
GI 447	11.12	1.75	dM4.5	3.3	364	0.080	0.017	41	3	-0.34	0.19	51.8	0.7
GI 449	3.61	0.55	F9 V	10.9	417	0.344	0.030	264	11	-0.63	0.07	170.9	24.3
GI 450	9.73	1.51	M1 Ve	8.6	377	0.069	0.015	37	6	-0.19	0.20	50.2	4.4
GI 452.4	10.52	1.39	M0 Ve	28.7	395	0.019	0.009	9	12	-0.75	0.33	8.2	8.1
GI 452.5A	7.29	0.64	G5 V	31.0	282	0.234	0.032	128	4	-0.28	0.13	159.9	183.3
GI 452.5B	7.70			31.0	282	0.234	0.032	128	4	-0.28	0.13	159.9	183.3
GI 454.2A	7.35	0.59	G0 V	56.2	163	0.162	0.034	61	12	0.32	0.20	162.5	613.6
GI 454.2B	8.10			56.2	163	0.162	0.034	61	12	0.32	0.20	162.5	613.6
GI 455	12.84	1.75	M3	20.2	478	0.089	0.017	38	10	-0.75	0.13	38.6	18.9
HD 104731	5.15	0.41	F6 V	24.2	173	0.067	0.023	14	30	-0.32	0.31	44.4	31.1
GI 455.1	9.99	1.34	K5 V	22.5	92	0.125	0.042	13	29	0.20	0.32	117.4	71.3
*GI 455.2	4.15	0.34	F2 III	19.7	374	0.372	0.032	522	2	-0.05	0.09	299.3	139.0
GI 455.3	4.02	0.32	F2 III-IV	14.8	292	1.362	0.100	663	8	-0.34	0.07	886.4	231.4
Wo 9390 A	6.81	0.66	G2 V	26.5	408	0.025	0.010	8	52	-1.00	1.35	7.5	6.3
Wo 9390 B	9.20		K5	26.5	408	0.025	0.010	8	33	-1.00	1.35	7.5	6.3
HD 105631	7.47	0.79	K0 V	24.3	445	0.039	0.012	14	6	-0.70	0.21	18.0	12.8
GI 456.1A	8.45	1.14	K5 V	20.1	279	0.043	0.015	13	20	-0.72	0.26	19.2	9.3

Name	<i>V</i>	<i>B - V</i>	Sp. type	<i>d</i> (pc)	Exp.	<i>CR</i>	$\pm CR$	Li	Δ	<i>hr</i>	Δhr	f_{x-14}	L_{x27}
Gl 456.1B	13.25	1.56	m	20.1	279	0.043	0.015	13	43	-0.72	0.26	19.2	9.3
HD 105963	8.03	0.88	K2	26.5	421	0.150	0.021	96	11	-0.41	0.12	92.2	77.6
LTT 13390	8.23		K3	31.5	421	0.150	0.021	96	23	-0.41	0.12	92.2	109.7
G122-074	12.91		m	21.8	318	0.072	0.018	28	10	-0.15	0.24	53.9	30.6
GJ 1154 AB	13.73	1.77	m	8.4	332	0.098	0.020	43	12	-0.24	0.19	69.2	5.8
San 39	14.15	1.62	dM4-5e	19.7	397	0.051	0.014	25	20	-0.52	0.19	28.1	13.1
GJ 1156	13.81	1.88	dM e	6.5	400	0.131	0.020	67	6	-0.25	0.15	91.3	4.7
HD 108421	8.89	1.02	K3 V	27.5	439	0.032	0.012	11	14	-0.50	0.24	18.3	16.7
G148-059	14.88	1.73	dM5 e	27.5	448	0.027	0.010	9	9	-0.33	0.31	18.0	16.3
LTT 4730	10.96	1.51	M2	17.3	58	0.218	0.066	17	71	-0.32	0.29	143.9	51.7
LP 735-11	11.00		g	17.3	58	0.218	0.066	17	56	-0.32	0.29	143.9	51.7
G123-035	12.90		m	14.4	487	0.146	0.020	94	8	-0.39	0.12	91.1	22.6
LP 377-100	14.18	1.60	dM5	20.4	459	0.092	0.016	57	9	0.21	0.18	87.0	43.3
Gl 469.2A	6.46	0.58	G0 V	25.0	257	0.620	0.050	432	4	-0.19	0.08	452.9	338.6
Gl 469.2B	9.20			25.0	257	0.620	0.050	432	4	-0.19	0.08	452.9	338.6
GJ 1160	8.12	0.93	K2 V	23.8	392	0.060	0.015	21	17	-0.04	0.24	48.5	32.7
Gl 471.2	4.30	0.37	F0 IV	18.2	231	0.209	0.032	86	4	-0.48	0.13	120.5	47.8
Steph 1021	12.90	1.56	M4	21.1	439	0.127	0.020	88	6	-0.27	0.14	87.7	46.7
Gl 473 A	13.04	1.83	dM5.5e	4.4	430	0.239	0.027	147	12	-0.44	0.09	142.6	3.3
Gl 473 B	13.30		M7	4.4	430	0.239	0.027	147	12	-0.44	0.09	142.6	3.3
Gl 475	4.27	0.59	G0 V	8.4	509	0.023	0.008	12	40	-1.00	0.39	7.0	0.6
GJ 1161 A	7.91	1.04	K4 V	21.6	220	0.050	0.021	7	20	-0.86	0.30	18.9	10.6
GJ 1161 B	11.91	1.60		21.6	220	0.050	0.021	7	77	-0.86	0.30	18.9	10.6
Gl 479	10.67	1.54	M3	9.7	312	0.132	0.023	59	7	-0.55	0.14	71.4	8.0
Gl 479.1	6.96	0.59	dG2 e	35.8	488	0.107	0.016	74	8	-0.13	0.16	81.5	125.2
G123-049	12.14		m	25.6	439	0.103	0.020	53	11	-0.33	0.15	67.4	52.7
LTT 13593	14.81	1.63	m	21.1	467	0.025	0.010	8	5	-0.61	0.26	12.5	6.7
Gl 482 A	3.46	0.36	F0 V	11.8	146	2.039	0.121	888	11	-0.11	0.06	1575.5	264.0
Gl 482 B	3.52		F0 V	11.8	146	2.039	0.121	888	11	-0.11	0.06	1575.5	264.0
HD 110463	8.29	0.95	K3 V	23.2	348	0.061	0.016	28	8	-0.27	0.23	41.9	27.0
Gl 483	7.04	0.94	K3 V	15.1	320	0.158	0.025	82	11	-0.52	0.13	88.0	23.9
GJ 1165	7.94	0.96	K2 V	21.2	324	0.081	0.019	29	10	-0.42	0.19	49.3	26.5
WD1246+586	15.56		DC8 :	18.5	352	0.516	0.041	418	20	-0.42	0.07	313.8	128.7
Gl 486.1	6.31	0.70	G7 V	17.2	424	0.133	0.021	77	14	-0.55	0.12	71.9	25.4
W ₀ 9417	5.85	0.46	F6 V	24.2	479	0.503	0.034	565	5	-0.19	0.06	367.7	256.7
Gl 487	10.90	1.64	M3	10.2	478	0.226	0.025	159	8	-0.22	0.10	161.8	20.1
Gl 488	8.49	1.40	M0.5Ve	10.8	221	0.061	0.021	12	36	-0.29	0.31	41.5	5.8
W ₀ 9421	6.11	0.50	F5 V	32.5	341	0.135	0.023	61	9	-0.40	0.14	83.8	105.6
Gl 488.1	4.26	0.21	A7 III	47.6	333	0.021	0.010	8	19	-0.44	0.42	12.3	33.4
Gl 490 A	10.68	1.44	M0 Ve	18.1	521	0.838	0.042	999	3	-0.22	0.05	598.5	234.1
Gl 490 B	13.20	1.64	dM4 e	18.1	521	0.838	0.042	999	18	-0.22	0.05	598.5	234.1
Gl 493.1	13.40	1.75	dM5 e	8.1	272	0.140	0.025	68	5	-0.16	0.18	104.5	8.2
*LTT 4974	10.95		dM2	16.8	638	0.010	0.004	11	14	-0.75	0.80	4.2	1.4
Gl 494	9.75	1.47	dM1.5e	11.4	177	1.566	0.099	705	10	-0.01	0.06	1293.0	202.1
Gl 498	9.30	1.17	dK8	21.9	516	0.023	0.009	8	12	-0.35	0.30	15.0	8.6
Gl 499 A	9.44	1.29	dM0	18.6	493	0.151	0.019	130	7	-0.40	0.12	93.4	38.6
Gl 499 B	14.90			18.6	493	0.151	0.019	130	7	-0.40	0.12	93.4	38.6
GJ 1167 A	14.18	1.72	dM5	11.5	508	0.098	0.016	76	3	-0.12	0.16	75.0	12.0
Gl 501 A	4.98	0.45	F5 V	18.3	244	0.876	0.063	538	9	-0.38	0.06	551.7	221.4
Gl 501 B	5.17		F5 V	18.3	244	0.876	0.063	538	9	-0.38	0.06	551.7	221.4
Gl 501.1	8.16	0.58	F5 IV	107.5	506	0.886	0.044	999	6	0.04	0.05	755.2	10447.1
Gl 501.2	4.85	0.70	G3 V	20.5	282	0.100	0.022	34	9	-0.70	0.15	45.9	23.1
Gl 502	4.26	0.57	G0 V	9.2	504	0.255	0.037	78	10	-0.73	0.09	113.2	11.4
Gl 503.2	6.83	0.60	G1 V	25.7	634	0.176	0.019	195	4	-0.36	0.09	112.7	89.1
Gl 504	5.20	0.58	G0 V	18.0	331	1.122	0.087	415	9	-0.14	0.08	849.1	327.5
Gl 505 A	6.59	0.94	K1 V	11.2	279	0.143	0.027	48	13	-0.65	0.13	69.5	10.5
Gl 505 B	9.60		M1 V	11.2	279	0.143	0.027	48	13	-0.65	0.13	69.5	10.5
HD 115781	8.13	1.14	K1 V	416.7	477	0.071	0.015	40	33	0.29	0.22	70.3	14603.9
Gl 508 A	8.94	1.48	dM1.5e	10.4	554	0.050	0.012	32	12	-0.44	0.20	29.8	3.8
Gl 508 B	9.80			10.4	554	0.050	0.012	32	12	-0.44	0.20	29.8	3.8
LHS 2729	12.90		m	13.4	309	0.137	0.024	56	4	-0.31	0.16	91.0	19.5
Gl 509 A	9.52	1.33	dM0	18.5	428	0.026	0.010	11	23	-1.00	0.35	7.9	3.2
Gl 509 B	9.80		dK6	18.5	428	0.026	0.010	11	23	-1.00	0.35	7.9	3.2
Gl 509.1	9.75	1.26	M0 V	25.1	697	0.198	0.019	222	11	-0.36	0.08	126.9	95.8
HD 116656	2.25	0.02	dA1 p	24.0	545	0.019	0.008	8	57	-0.34	0.36	12.5	8.6
HD 116657	3.95	0.13	A1 m	24.0	545	0.019	0.008	8	38	-0.34	0.36	12.5	8.6
HD 116842	4.01	0.16	A5 V	24.9	552	0.026	0.010	13	2	0.24	0.34	25.4	18.8
LHS 2739	13.60		M4		300	0.099	0.021	32	4	0.00	0.22	82.2	
Gl 514	9.05	1.50	M1 V	7.6	311	0.058	0.016	21	10	-0.40	0.26	35.8	2.5
G165-008	11.95	1.57	M4 e	7.5	450	0.410	0.032	335	6	-0.33	0.07	269.1	17.9
Gl 516 A	12.01	1.53	dM3.5e	16.3	340	0.076	0.018	32	23	-0.48	0.18	43.6	13.8
Gl 516 B	12.30		dM3.5e	16.3	340	0.076	0.018	32	23	-0.48	0.18	43.6	13.8
GJ 2102	7.98	1.00	K0	18.5	353	0.046	0.015	16	24	-0.36	0.26	29.5	12.0
Gl 517	9.31	1.21	K5	19.8	325	1.061	0.060	793	6	-0.21	0.05	763.6	358.2
HD 118098	3.37	0.11	A3 V	22.5	252	0.025	0.012	10	15	-0.26	0.45	17.5	10.6
Gl 519	9.04	1.42	dM1	10.9	578	0.029	0.010	12	29	-0.57	0.21	15.4	2.2
Gl 520 A	10.17	1.40	dM0.5	21.9	557	0.030	0.011	10	14	-0.74	0.21	13.3	7.6
Gl 520 B	11.00			21.9	557	0.030	0.011	10	14	-0.74	0.21	13.3	7.6
GJ 1175	6.98	0.86	K1 V	15.6	304	0.191	0.028	72	21	-0.33	0.14	125.6	36.6
Gl 521.2A	6.33	0.54	F7 V	25.3	541	0.365	0.029	372	4	-0.15	0.08	274.5	209.4

Name	V	$B - V$	Sp. type	$d(\text{pc})$	Exp.	CR	$\pm CR$	Li	Δ	hr	Δhr	f_{x-14}	L_{x27}
Gl 521.2B	10.46	1.36		25.3	541	0.365	0.029	372	21	-0.15	0.08	274.5	209.4
LHS 2783	13.50		m	13.0	338	0.060	0.016	26	6	-0.78	0.19	25.1	5.1
Gl 525.1	4.23	0.38	F3 IV	19.3	283	0.615	0.049	404	6	0.02	0.08	517.9	230.0
GJ 1177 A	8.94	1.32	K5 V	16.4	271	0.115	0.025	27	11	-0.52	0.18	63.9	20.5
GJ 1177 B	9.12	1.36		16.4	271	0.115	0.025	27	10	-0.52	0.18	63.9	20.5
Gl 527 A	4.50	0.48	F7 V	15.6	376	0.563	0.061	179	11	-0.54	0.09	306.5	89.3
Gl 527 B	11.00		M2	15.6	376	0.563	0.061	179	11	-0.54	0.09	306.5	89.3
LTT 14031	14.34		m	14.6	330	0.056	0.016	26	28	0.08	0.27	49.3	12.7
Gl 528 A	7.61	1.12	K4 V	13.6	453	0.127	0.020	87	3	-0.44	0.12	76.2	17.0
Gl 528 B	8.03		dK6	13.6	453	0.127	0.020	87	3	-0.44	0.12	76.2	17.0
Gl 530	6.44	0.69	G5 V	19.9	217	0.063	0.020	16	5	-0.74	0.26	27.6	13.1
*Gl 531	7.38	0.90	K1 V	16.4	426	0.146	0.019	94	15	-0.19	0.10	106.3	34.3
G150-046	11.63	1.50	M2	15.8	361	0.029	0.011	10	21	-1.00	0.99	8.8	2.6
Gl 534	2.68	0.58	G0 IV	11.3	377	0.144	0.023	55	13	-0.65	0.13	70.0	10.8
LHS 2836	13.00		K2 :	9.5	313	0.195	0.027	113	8	-0.33	0.13	127.7	13.8
Gl 536	9.70	1.46	M1	10.2	398	0.033	0.011	11	67	-0.83	0.27	12.9	1.6
13 59 54 +13 55.9	10.65	1.47	dM0.5	19.5	296	0.025	0.011	8	9	-0.65	0.31	12.1	5.5
LHS 2852	12.15	1.70	M0.5		286	0.153	0.026	72	6	-0.43	0.14	92.3	
Gl 537 A	9.85	1.48	dM3 e	11.3	390	0.083	0.018	41	5	-0.46	0.17	48.6	7.4
Gl 537 B	9.95		dM3 e	11.3	390	0.083	0.018	41	5	-0.46	0.17	48.6	7.4
HD 124106	7.93	0.86	K1 V	23.1	294	0.032	0.012	14	8	-1.00	1.03	9.6	6.1
Gl 540.2	13.86	1.53	dM5.5e	12.4	282	0.199	0.029	142	9	-0.17	0.13	147.4	27.3
HD 124498	10.40	1.28	K4 V	26.5	308	0.780	0.052	665	16	-0.19	0.07	570.0	477.3
LTT 5581	13.96	1.60	m	26.5	308	0.780	0.052	665	50	-0.19	0.07	570.0	477.3
HD 124642	8.04	1.08	K4	17.3	479	0.052	0.013	24	19	-0.43	0.23	31.5	11.3
*Gl 540.3	6.31	0.60	G4 V	21.0	522	0.205	0.020	156	6	-0.38	0.10	129.2	68.5
Wo 9473	4.08	0.52	F6 III	21.4	339	0.946	0.078	395	8	-0.03	0.08	771.2	423.1
Wo 9474 A	4.75	0.20	A7 V	29.9	686	0.058	0.012	41	43	-0.47	0.15	33.9	36.1
Wo 9474 B	8.23	0.82	K1 V	29.9	686	0.058	0.012	41	7	-0.47	0.15	33.9	36.1
G165-061	13.10		m	16.1	484	0.114	0.018	75	8	-0.45	0.13	67.8	21.0
Gl 541.2	10.25	1.44	dM0 p	18.7	892	0.089	0.012	85	61	-0.28	0.12	61.1	25.4
Gl 542.2	9.10	1.30	K5	21.5	329	0.031	0.012	10	27	-0.34	0.36	20.2	11.2
HD 125451	5.41	0.38	dF1	26.1	234	0.202	0.033	70	11	-0.14	0.16	152.6	124.4
Steph 1145	12.31	1.51	M0:e:	20.3	614	0.159	0.018	148	10	-0.13	0.11	121.4	59.8
Gl 546	8.55	1.26	K8 V	14.4	556	0.059	0.013	29	16	-0.29	0.18	40.1	10.0
Gl 548 A	9.75	1.44	dM1	16.8	425	0.045	0.012	26	36	-0.12	0.26	34.8	11.8
Gl 548 B	10.00	1.46	dM2	15.8	425	0.045	0.012	26	7	-0.12	0.26	34.8	10.4
Gl 549 A	4.06	0.50	F7 V	14.6	724	1.996	0.055	999	4	0.02	0.03	1679.8	427.1
Gl 549 B	11.50	1.50	M3	14.6	724	1.996	0.055	999	74	0.02	0.03	1679.8	427.1
WD1424+240	15.41		DC8	17.2	384	0.343	0.032	305	12	0.03	0.10	290.9	103.5
GJ 1183 A	13.95	1.65	m	16.2	331	0.131	0.022	68	23	-0.17	0.16	96.7	30.4
GJ 1183 B	14.03	1.68	m	16.2	331	0.131	0.022	68	9	-0.17	0.16	96.7	30.4
Gl 550.2A	4.83	0.72	G2 IV	41.5	247	1.211	0.071	999	8	0.07	0.06	1051.3	2165.6
Gl 550.2B	9.00		G4 V	41.5	247	1.211	0.071	999	8	0.07	0.06	1051.3	2165.6
Gl 551	11.05	1.83	dM5 e	1.3	374	1.374	0.111	445	3	-0.41	0.07	843.2	1.7
HD 127068	8.38		G5	102.0	466	0.401	0.032	347	7	0.20	0.08	375.5	4678.5
Gl 554	8.70	1.04	dK5	22.0	625	0.019	0.007	9	11	-0.74	0.25	8.2	4.8
LP 440-38	13.61		m	16.7	361	0.047	0.015	19	18	-0.52	0.22	25.9	8.6
HD 128642	6.91	0.76	G5	19.6	747	0.032	0.009	11	13	-1.00	0.17	9.8	4.5
Gl 556	7.23	0.99	K3 V	13.4	775	0.040	0.010	20	33	-0.86	0.11	15.1	3.3
Gl 557	4.46	0.36	F2 V	15.5	457	0.171	0.022	112	2	-0.32	0.12	112.8	32.2
HD 128311	7.50	0.99	K0	16.6	345	0.149	0.024	88	9	-0.29	0.14	100.8	33.2
G223-074	11.74		m	14.7	627	0.122	0.017	95	6	-0.31	0.12	81.7	21.1
Gl 559 A	0.01	0.64	G2 V	1.3	420	3.177	0.212	589	7	-0.98	0.02	990.0	2.2
Gl 559 B	1.34	0.84	K0 V	1.3	420	3.177	0.212	589	7	-0.98	0.02	990.0	2.2
HD 128400	6.73		G5 V	20.3	272	0.140	0.026	57	11	-0.50	0.16	79.4	39.2
Gl 559.1	7.54	0.61	dG0 e	33.9	582	0.981	0.042	999	1	-0.14	0.04	742.4	1020.7
Wo 9491	3.88	0.38	F2 III	18.7	337	0.642	0.046	588	3	0.17	0.07	591.5	247.3
Wo 9492	10.83	1.55	M3	10.8	1069	0.022	0.006	18	25	-0.05	0.25	17.7	2.5
*Gl 561.1A	5.10	0.34	F2 III-IV	30.4	454	0.114	0.016	35	30	-0.22	0.12	81.7	90.3
*Gl 561.1B	7.14		dF9	30.4	454	0.114	0.016	35	15	-0.22	0.12	81.7	90.3
HD 130307	7.78	0.90	G8 V	19.7	350	0.031	0.012	8	7	-0.11	0.35	24.0	11.1
Gl 563.4	5.15	0.41	F5 IV-V	23.6	379	0.283	0.031	189	11	-0.30	0.10	190.0	127.1
Gl 564	5.85	0.56	G2 V	18.0	529	0.407	0.031	427	13	-0.35	0.07	262.5	101.2
HD 131023	7.40	0.76	dG5	27.2	330	0.089	0.021	26	6	-0.32	0.21	58.9	52.3
LTT 14398	8.90		k	27.2	330	0.089	0.021	26	1	-0.32	0.21	58.9	52.3
*Gl 565	7.83	1.00	K5 V	17.0	1207	0.024	0.004	47	7	-0.78	0.11	9.9	3.4
Gl 566 A	4.70	0.73	G8 Ve	6.7	400	2.440	0.183	416	6	-0.31	0.07	1626.7	87.3
Gl 566 B	6.97	1.16	K4 Ve	6.7	400	2.440	0.183	416	6	-0.31	0.07	1626.7	87.3
Gl 567	6.02	0.84	K2 V	11.5	398	0.363	0.034	245	14	-0.48	0.08	209.2	33.3
Gl 568 A	12.19	1.61	M3.5	10.2	451	0.040	0.013	17	17	-0.45	0.22	23.6	2.9
Gl 568 B	12.70			10.2	451	0.040	0.013	17	17	-0.45	0.22	23.6	2.9
Gl 569 AB	10.20	1.48	dM0 e	9.8	385	0.489	0.038	361	5	-0.41	0.07	300.3	34.6
LP 222-015	14.67		m	23.8	655	0.020	0.008	7	26	0.23	0.40	18.6	12.6
HD 133002	5.64	0.68	F9 V	43.3	753	0.115	0.014	146	9	-0.20	0.12	83.7	187.8
LHS 3001	15.50		M5	21.6	389	0.015	0.007	9	68	-0.11	0.42	11.8	6.6
LHS 3002	18.60		M7 :	21.6	389	0.015	0.007	9	83	-0.11	0.42	11.8	6.6
*Gl 570 A	5.75	1.10	K5 Ve	5.9	820	0.200	0.016	378	6	-0.77	0.06	84.5	3.5
*Gl 570 B	8.00	1.50	M2 V	5.9	820	0.200	0.016	378	27	-0.77	0.06	84.5	3.5
Wo 9503	4.49	0.32	F0 V	27.9	406	0.023	0.010	8	23	-0.70	0.35	10.5	9.8

Name	V	$B - V$	Sp. type	$d(\text{pc})$	Exp.	CR	$\pm CR$	Li	Δ	hr	Δhr	f_{x-14}	L_{x27}
Gl 570.1	6.35	0.71	G5 V	24.5	349	0.017	0.008	8	29			14.0	10.1
HD 132254	5.63	0.50	F8 V	24.8	740	0.027	0.009	9	29	-0.10	0.28	20.7	15.2
Gl 572	9.13	1.43	dM0	11.7	775	0.147	0.016	172	13	-0.41	0.09	90.1	14.7
Gl 575 A	5.19	0.65	F9 V n	12.8	612	3.414	0.076	999	12	-0.16	0.02	2547.5	495.9
Gl 575 B	5.96		dG2	12.8	612	3.414	0.076	999	12	-0.16	0.02	2547.5	495.9
Gl 577	8.42	0.68	dG5 e	44.2	876	0.103	0.013	123	7	-0.09	0.11	81.0	189.7
Gl 578	4.93	0.43	F5 V	19.7	380	0.208	0.026	149	2	-0.48	0.10	120.2	55.9
G179-020	13.35		m	13.5	589	0.047	0.011	33	19	-0.46	0.18	27.5	6.0
HD 136351	5.00	0.50	F8 V	34.1	392	0.156	0.022	110	0	-0.10	0.14	121.1	168.8
GJ 2112 AB	13.28	1.70	M3 :		378	0.034	0.011	18	10	0.44	0.33	36.6	
W0 9520	10.11	1.51	dM0 e	11.4	179	0.994	0.080	427	16	-0.24	0.08	699.9	108.6
Gl 584 A	5.62	0.58	G2 V	18.6	376	0.148	0.024	76	4	-0.78	0.10	61.7	25.6
Gl 584 B	5.96		G2 V	18.6	376	0.148	0.024	76	4	-0.78	0.10	61.7	25.6
Gl 586 A	6.92	0.81	K2 V	19.9	380	0.146	0.023	82	57	-0.41	0.14	89.4	42.3
Gl 586 B	7.58	0.92	K2 V	20.8	380	0.146	0.023	82	8	-0.41	0.14	89.4	46.2
Gl 588	9.31	1.52	M3	5.9	416	0.040	0.013	13	22	-1.00	0.16	12.0	0.5
Gl 593 A	7.43	0.91	K2 V	21.8	420	0.046	0.014	14	18	-0.39	0.24	28.7	16.3
Gl 593 B	7.60			21.8	420	0.046	0.014	14	18	-0.39	0.24	28.7	16.3
Gl 594	4.64	0.40	F5 IV-V	17.5	420	0.523	0.037	476	14	-0.29	0.07	354.3	130.0
Gl 596.1A	5.86	0.68	G5 V	14.7	492	0.129	0.018	96	3	-0.65	0.11	62.7	16.1
Gl 596.1B	12.00			14.7	492	0.129	0.018	96	3	-0.65	0.11	62.7	16.1
Gl 598	4.43	0.60	G0 V	11.8	503	0.062	0.014	30	19	-0.72	0.13	27.9	4.6
Gl 599 A	6.01	0.72	G6 V	15.2	394	0.147	0.023	67	4	-0.73	0.11	65.2	18.1
Gl 599 B	12.78	0.33	DA7	15.2	394	0.147	0.023	67	4	-0.73	0.11	65.2	18.1
HD 141272	7.43	0.81	G8 V	21.4	490	0.187	0.022	149	3	-0.30	0.12	125.5	68.6
G179-057	13.16	1.64	m	17.0	271	0.023	0.012	8	21	-0.58	0.29	12.0	4.2
Gl 600	9.36	1.42	dM0	22.6	540	0.022	0.008	9	12	-0.72	0.32	9.9	6.1
Gl 601 A	2.84	0.29	F2 IV	12.3	365	0.144	0.025	58	8	-0.91	0.06	50.3	9.1
HD 142267	6.10	0.60	G1 V	17.5	546	0.016	0.007	7	14	-0.68	0.33	7.5	2.7
G180-011	13.68		m	11.1	325	0.155	0.025	97	9	0.08	0.16	135.8	20.2
W0 9531	5.45	0.33	F0 IV	41.5	269	0.036	0.014	10	27	-0.80	0.45	14.8	30.4
Gl 603	3.85	0.48	F6 V	11.1	560	0.035	0.012	10	7	-0.90	0.14	12.5	1.9
HD 143313	8.33	1.00	K2 V	87.7	630	0.643	0.034	999	9	0.07	0.05	557.8	5135.6
Gl 606	10.50	1.51	dM0	13.9	198	0.052	0.020	9	28	-0.73	0.38	23.2	5.4
HD 143333	5.47	0.52	F8 V	32.8	450	0.087	0.017	49	13	-0.27	0.18	59.6	76.7
Gl 609.1	4.01	0.52	F8 IV-V	20.9	1603	0.750	0.023	999	1	-0.09	0.03	587.5	307.6
W0 9540 A	4.84	0.45	F6 IV-V	23.3	458	0.253	0.025	233	9	-0.32	0.09	167.7	108.5
W0 9540 B	5.00		F6 IV-V	23.3	458	0.253	0.025	233	9	-0.32	0.09	167.7	108.5
W0 9540 C	7.30	0.75	G8 V	23.3	458	0.253	0.025	233	15	-0.32	0.09	167.7	108.5
W0 9541 A	7.46	0.74	G8 V	28.3	458	0.085	0.016	60	14	-0.64	0.14	41.9	40.2
W0 9541 B	8.03	0.84	K2 V	29.5	458	0.085	0.016	60	14	-0.64	0.14	41.9	43.6
16 07 47 +53 04.4	10.19	1.45	dM0	17.1	499	0.023	0.009	8	23	-0.04	0.33	18.5	6.5
Gl 615.2A	5.64	0.51	F8 V	21.7	764	9.487	0.115	999	6	0.07	0.01	8235.7	4636.4
Gl 615.2B	6.72		G1 V	21.7	764	9.487	0.115	999	6	0.07	0.01	8235.7	4636.4
Gl 616.2	9.96	1.48	dM1.5e	20.7	1036	0.916	0.032	999	14	-0.12	0.03	703.3	359.2
Gl 617 A	8.60	1.41	M0 Ve	10.7	1726	0.060	0.007	91	13	-0.50	0.10	33.9	4.6
Gl 617 B	10.72	1.49	M2.5	10.7	1726	0.060	0.007	91	53	-0.50	0.10	33.9	4.7
Gl 618 A	10.60	1.57	M3	8.5	368	0.029	0.011	10	17	-1.00	0.75	8.8	0.8
Gl 618 B	14.15	1.79	M5 :	8.5	368	0.029	0.011	10	17	-1.00	0.75	8.8	0.8
W0 9557 A	5.46	0.40	F3 IV-V	26.8	818	0.640	0.030	999	7	-0.16	0.04	477.5	410.6
W0 9557 B	11.00			26.8	818	0.640	0.030	999	7	-0.16	0.04	477.5	410.6
HD 148048	4.95	0.37	F3 V	29.9	912	0.030	0.007	19	61	-0.28	0.22	20.5	21.8
HD 147449	4.82	0.34	F0 V	27.3	439	0.043	0.013	14	11	-0.52	0.31	24.1	21.5
Gl 620.1A	5.39	0.63	G3/5 V	12.9	349	0.654	0.045	646	8	-0.26	0.07	453.6	89.9
Gl 620.1B	11.00	-0.14	DA2	12.8	355	0.688	0.068	192	16	-0.97	0.03	218.2	42.9
*Gl 621	8.40	0.96	K3 V	21.5	378	0.026	0.010	12	22	-0.89	0.16	9.2	5.1
Gl 624	4.91	0.55	G0 V	12.1	166	1.027	0.081	493	2	-0.23	0.08	728.2	127.7
Gl 624.1A	2.74	0.91	G8 III	26.9	1846	0.017	0.005	12	12	-0.81	0.12	6.7	5.8
Gl 624.1B	8.80		K2	26.9	1846	0.017	0.005	12	12	-0.81	0.12	6.7	5.8
LHS 3197	14.30		m	12.1	378	0.021	0.009	8	13	-0.66	0.28	10.0	1.7
Gl 625	10.12	1.61	dM2	6.6	724	0.019	0.007	9	10	-0.57	0.27	9.9	0.5
Gl 626.1	3.89	0.91	K0 IV	49.0	192	0.586	0.057	321	7	0.25	0.10	564.1	1621.8
Gl 627 A	7.68	0.85	K3 V	19.5	469	0.052	0.013	25	4	-0.68	0.18	24.2	11.1
Gl 627 B	7.85		K3 V	19.5	469	0.052	0.013	25	4	-0.68	0.18	24.2	11.1
Gl 628	10.08	1.58	M3.5	4.3	554	0.047	0.011	27	10	-0.96	0.16	15.3	0.3
W0 9566	8.85	0.88	K1	42.6	512	0.176	0.022	145	16	-0.11	0.12	136.1	295.0
Gl 630.1A	12.90	1.60	dM4 e	14.5	956	0.177	0.015	251	8	-0.30	0.08	118.7	29.7
Gl 630.1B	15.00	0.49	DQ8	14.5	956	0.177	0.015	251	22	-0.30	0.08	118.7	29.7
LP 275-68	12.95		m	12.1	590	0.169	0.019	144	15	-0.16	0.11	126.0	21.9
GJ 1204	13.80	1.65	m	15.3	477	0.041	0.012	11	31	-0.49	0.34	23.2	6.5
Gl 631	5.75	0.82	K0 Ve	9.8	603	0.258	0.032	148	3	-0.64	0.10	126.8	14.5
Gl 632	7.06	0.62	dG3	27.2	1096	0.123	0.012	249	4	-0.22	0.09	87.8	78.0
Gl 632.2A	10.02	1.15	K7	31.3	1089	0.015	0.005	11	9	0.36	0.36	15.3	18.0
Gl 632.2B	13.00		DA	31.3	1089	0.015	0.005	11	4	0.36	0.36	15.3	18.0
LP 625-34	13.69	1.70	m	11.2	631	0.058	0.012	36	16	-0.37	0.19	36.8	5.6
Gl 635 A	2.91	0.65	G0 IV	10.8	494	0.128	0.019	77	15	-0.72	0.09	57.4	8.0
Gl 635 B	5.40		K0 V	10.8	494	0.128	0.019	77	15	-0.72	0.09	57.4	8.0
G240-023	15.65	1.95	m	13.4	2374	0.071	0.007	175	11	-0.13	0.08	53.7	11.5
Gl 638	8.11	1.37	K7 V	9.8	468	0.026	0.009	11	39	-1.00	1.49	7.9	0.9
W0 9578	4.85	0.38	F2 V	26.7	777	0.235	0.019	343	9	-0.03	0.08	191.5	163.8

Name	<i>V</i>	<i>B</i> - <i>V</i>	Sp. type	<i>d</i> (pc)	Exp.	<i>CR</i>	$\pm CR$	Li	Δ	<i>hr</i>	Δhr	f_{x-14}	L_{x27}
G169-029	14.08	1.75	m	10.0	742	0.063	0.011	47	10	-0.35	0.15	40.5	4.9
Gl 641	6.64	0.76	G8 V	16.9	491	0.317	0.028	286	9	-0.07	0.09	251.8	86.6
Gl 643	11.80	1.69	sdM4	6.5	445	3.968	0.245	906	75	-0.26	0.06	2750.6	138.8
Gl 644 A	9.69	1.57	M3	5.7	445	3.968	0.245	906	10	-0.26	0.06	2750.6	108.4
Gl 644 B	9.90			5.7	445	3.968	0.245	906	10	-0.26	0.06	2750.6	108.4
GJ 1207	12.28	1.60	dM3.5	9.6	472	0.374	0.043	180	6	-0.46	0.10	219.7	24.1
Gl 648	4.89	0.48	F6 V	15.1	2622	0.406	0.013	999	1	-0.42	0.03	246.9	67.2
Gl 649.1A	7.83	0.98	dK8	18.0	823	0.077	0.012	63	6	-0.57	0.11	40.5	15.6
Gl 649.1B	11.19	1.47		18.0	823	0.077	0.012	63	6	-0.57	0.11	40.5	15.6
HD 153580	5.29	0.50	F6 V	26.3	243	0.255	0.036	100	10	-0.26	0.14	176.7	146.4
Wo 9582 A	8.65	1.04	K4 V	25.2	1056	0.026	0.006	20	23	-1.00	0.13	7.8	5.9
Wo 9582 B	10.31	1.40	K4	24.9	1056	0.026	0.006	20	12	-1.00	0.13	7.8	5.8
Gl 654	10.08	1.44	M3.5V	10.6	386	0.023	0.011	8	65	-0.33	0.40	15.0	2.0
Gl 654.1	6.00	0.58	F9 V	20.4	496	0.230	0.023	193	1	-0.48	0.09	132.6	65.8
Gl 654.2	7.09	0.94	K0 V	227.3	539	0.012	0.006	8	79			9.8	606.0
Wo 9584 A	5.63	0.47	F7 V	27.0	1270	0.484	0.021	999	5	-0.25	0.04	338.4	294.1
Wo 9584 B	5.73		F7 V	27.0	1270	0.484	0.021	999	5	-0.25	0.04	338.4	294.1
Wo 9584 C	13.50		M3 :	27.0	1270	0.484	0.021	999	5	-0.25	0.04	338.4	294.1
Gl 657	3.33	0.41	F0 IVn	21.9	304	0.108	0.021	43	17	-0.88	0.12	39.4	22.7
Gl 659 A	8.85	1.16	dK8	21.2	1214	0.053	0.008	60	9	-0.51	0.11	29.7	16.0
Gl 659 B	9.34	1.25	dK8	20.9	1214	0.053	0.008	60	17	-0.51	0.11	29.7	15.5
HD 155902	6.98	0.70	G5	28.2	1510	0.028	0.006	26	15	-0.81	0.11	11.1	10.6
Gl 661 A	9.96	1.49	M3	6.3	1145	0.058	0.009	65	22	-0.68	0.11	27.3	1.3
Gl 661 B	10.40		M3.5	6.3	1145	0.058	0.009	65	22	-0.68	0.11	27.3	1.3
Gl 663 A	5.07	0.85	K1 Ve	6.0	291	0.854	0.058	664	9	-0.58	0.05	447.2	19.2
Gl 663 B	5.11	0.86	K1 Ve	6.0	291	0.854	0.058	664	7	-0.58	0.05	447.2	19.2
Gl 664	6.33	1.16	K5 Ve	6.0	288	0.255	0.032	157	3	-0.60	0.11	130.6	5.6
Gl 666 A	5.53	0.77	G8 V	8.8	251	0.029	0.013	8	44	-0.26	0.48	20.1	1.9
Gl 666 B	8.69	1.41	M0 V	8.8	251	0.029	0.013	8	44	-0.26	0.48	20.1	1.9
Gl 667 A	6.29	1.04	K3 V	7.2	307	0.206	0.029	120	5	-0.61	0.11	104.4	6.4
Gl 667 B	7.20		K5 V	7.2	307	0.206	0.029	120	5	-0.61	0.11	104.4	6.4
Gl 667 C	10.24	1.57	M2.5	7.2	307	0.206	0.029	120	17	-0.61	0.11	104.4	6.4
BPM 78873	10.59	1.44	K7	20.7	445	0.035	0.011	13	23	-0.56	0.25	18.5	9.5
LTT 15124	13.02		m	19.5	613	0.031	0.009	19	11	-0.57	0.22	16.2	7.4
Gl 669 A	11.42	1.55	dM4 e	10.7	691	0.594	0.031	999	13	-0.16	0.05	443.5	60.3
Gl 669 B	12.97	1.64	dM5 e	10.7	691	0.594	0.031	999	7	-0.16	0.05	443.5	60.3
Gl 670 A	4.41	0.39	F2 V	17.4	318	0.112	0.021	52	18	-0.60	0.16	57.7	20.9
Gl 670 B	8.90		K3	17.4	318	0.112	0.021	52	18	-0.60	0.16	57.7	20.9
Gl 673	7.53	1.36	K7 V	7.7	445	0.090	0.018	40	3	-0.37	0.18	57.5	4.1
Gl 674	9.37	1.53	M3	4.5	193	0.267	0.041	76	2	-0.60	0.13	136.8	3.4
LTT 15193	13.35		m	21.2	883	0.038	0.008	30	9	-0.37	0.20	23.9	12.9
Gl 679	6.56	0.65	G5 V	23.7	840	0.024	0.007	17	17	-0.80	0.15	10.0	6.7
Gl 681	2.08	0.15	A5 III	14.3	542	0.124	0.016	111	7	-0.60	0.11	63.7	15.6
Gl 683.1	7.17	0.65	G5 V	33.6	234	0.129	0.027	46	22	-0.39	0.18	80.3	108.2
Gl 684 A	5.34	0.56	G0 Va	14.1	2942	0.345	0.012	999	10	-0.49	0.03	197.2	46.8
Gl 684 B	8.06	1.10	K3 V	14.1	2942	0.345	0.012	999	10	-0.49	0.03	197.2	46.8
Gl 685	9.97	1.47	M1 Ve	14.1	2947	0.023	0.004	55	8	-0.58	0.11	12.0	2.9
Gl 686.1A	10.00	1.33	dM0 e	22.1	638	0.025	0.008	14	31	-0.56	0.26	13.2	7.8
Gl 686.1B	10.22	1.38		22.1	638	0.025	0.008	14	31	-0.56	0.26	13.2	7.8
Gl 686.2	4.77	0.40	F2 V	21.9	164	0.128	0.033	32	13	-0.31	0.27	85.1	48.8
Gl 687	9.18	1.50	M3.5 V	4.5	5788	0.062	0.004	374	8	-0.63	0.05	30.8	0.8
Gl 688	6.52	0.96	K3 V	10.7	440	0.048	0.013	19	11	-0.71	0.18	21.9	3.0
Gl 689	8.62	1.10	dK8	19.0	2894	0.017	0.003	23	14	-0.65	0.14	8.3	3.6
HD 160922	4.80	0.43	F5 V	23.5	4848	0.465	0.010	999	8	-0.28	0.02	317.8	209.5
AC+61:27026A	10.28	1.23	dK8	24.5	2881	0.634	0.016	999	7	-0.15	0.02	476.7	342.6
AC+61:27026B	14.70			24.5	2881	0.634	0.016	999	10	-0.15	0.02	476.7	342.6
Gl 690 A	9.20	1.10	dM0	23.9	3280	0.011	0.003	18	10	-0.82	0.12	4.4	3.0
Wo 9599	8.37	0.93	K0	26.5	5029	0.036	0.003	179	1	-0.38	0.08	22.5	18.9
G140-009	10.67		M2	19.7	350	0.060	0.016	22	5	-0.70	0.20	27.8	12.9
Gl 694	10.47	1.53	dM3.5	9.5	1109	0.024	0.006	17	7	-0.79	0.15	9.7	1.0
Gl 694.1A	4.58	0.42	F5 IV-V	22.0	3397	0.125	0.007	600	9	-0.50	0.04	70.8	41.1
Gl 694.1B	5.79	0.53	F8 V	22.3	3397	0.125	0.007	600	22	-0.50	0.04	70.8	42.2
Gl 694.2	10.72	1.49	dM1.5	22.5	1279	0.009	0.004	8	28	0.06	0.37	7.9	4.8
Gl 695 A	3.42	0.75	G5 IV	8.4	718	0.197	0.019	232	6	-0.86	0.06	73.9	6.2
Gl 695 B	10.35	1.49	M3	8.4	718	0.197	0.019	232	27	-0.86	0.06	73.9	6.2
Gl 695 C	10.80		M4	8.4	718	0.197	0.019	232	27	-0.86	0.06	73.9	6.2
Gl 697	8.48	0.95	dK5	24.9	619	0.038	0.009	29	9	-0.34	0.21	24.7	18.3
HD 162521	6.36	0.45	F8 V	34.6	151	0.087	0.030	16	9	-0.49	0.34	49.6	71.0
Gl 698	9.22	1.18	dK8	23.0	271	0.030	0.013	9	26	-0.49	0.40	17.4	11.0
HD 163621	7.84		G5	30.9	880	1.875	0.047	999	5	-0.05	0.03	1508.4	1719.2
HD 163840	6.30	0.64	G2 V	28.6	651	0.020	0.007	14	35	-1.00	0.37	6.1	5.9
Gl 699	9.55	1.74	M5 V	1.8	399	0.030	0.011	13	11	-0.75	0.30	12.9	0.1
G204-039	11.79	1.56	m	13.6	1065	0.025	0.007	19	15	-0.58	0.19	13.2	2.9
Gl 699.2	4.62	0.38	F3 V	23.2	343	0.197	0.025	133	7	-0.04	0.13	159.3	102.6
Gl 700.1A	5.24	0.38	dF3	52.1	276	0.076	0.019	32	4	-0.14	0.24	57.5	186.7
Gl 700.1B	5.93			52.1	276	0.076	0.019	32	4	-0.14	0.24	57.5	186.7
Gl 701	9.38	1.52	dM2	7.8	310	0.031	0.012	10	17	-0.11	0.39	23.7	1.7
Gl 702 A	4.21	0.86	K0 Ve	5.1	347	1.649	0.127	410	7	-0.52	0.07	915.9	28.3
Gl 702 B	6.00	1.15	K5 Ve	5.1	347	1.649	0.127	410	7	-0.52	0.07	915.9	28.3
Gl 702.1	5.95	0.62	G5 V	17.4	124	0.585	0.075	131	12	-0.27	0.13	402.7	145.2

Name	<i>V</i>	<i>B</i> - <i>V</i>	Sp. type	<i>d</i> (pc)	Exp.	<i>CR</i>	$\pm CR$	Li	Δ	<i>hr</i>	Δhr	f_{x-14}	L_{x27}
Gl 702.2	6.80	0.62	G2 V	24.4	348	0.039	0.015	12	11	-0.38	0.36	24.6	17.5
GJ 1224	13.63	1.79	m	7.5	296	0.211	0.029	104	5	-0.45	0.12	124.8	8.5
Wo 9615 A	3.73	0.12	A4 V	25.4	401	0.021	0.010	7	31	-0.58	0.30	11.2	8.6
Wo 9615 B	14.00			25.4	401	0.021	0.010	7	31	-0.58	0.30	11.2	8.6
Gl 704 A	5.09	0.50	F7 V	15.6	719	0.016	0.006	9	17	-1.00	0.57	4.9	1.4
Gl 704 B	8.45	1.10	K5 V	15.6	719	0.016	0.006	9	17	-1.00	0.57	4.9	1.4
LP 390-16	13.32		m	13.9	554	0.300	0.025	308	11	0.00	0.08	249.1	57.2
Gl 708.1	5.03	0.38	F5 V	23.5	5748	0.242	0.007	999	6	-0.18	0.03	178.2	117.5
Gl 710	9.66	1.37	dM1	19.3	308	0.041	0.014	13	17	-0.16	0.39	30.2	13.5
G258-033	13.48	1.83	m	7.3	9325	0.056	0.003	494	2	-0.50	0.04	31.8	2.0
G021-013	11.84	1.56	g		321	0.019	0.009	8	31	-1.00	1.28	5.6	
Gl 713 AB	3.57	0.49	F7 V	8.1	2629	0.156	0.009	506	20	-0.76	0.04	66.7	5.2
Gl 716	6.81	0.85	K3 V	13.2	296	0.050	0.016	15	23	-0.22	0.37	35.6	7.4
G205-028	11.99		m	12.5	727	0.011	0.005	8	51	-0.73	0.33	4.8	0.9
Gl 719	8.10	1.22	K6 Ve	16.4	1085	2.414	0.048	999	2	-0.01	0.02	1993.2	643.0
LP 229-17	11.42	1.42	M3 p	7.7	703	0.019	0.006	17	24	-0.52	0.26	10.4	0.7
Gl 720 A	9.85	1.42	dM2	15.5	1183	0.014	0.005	14	7	-0.70	0.21	6.3	1.8
G141-021	12.46		M3.5	10.4	335	0.111	0.021	52	10	-0.43	0.19	66.8	8.6
Gl 722	5.86	0.68	G5 V	13.0	283	0.045	0.016	15	16	-0.67	0.21	21.4	4.3
Gl 722.1	8.34	0.82	dK0 e	28.5	1019	0.011	0.004	9	24	-0.76	0.30	4.6	4.5
GJ 1230 A	12.40	1.71	k-m	8.3	454	0.179	0.022	156	13	-0.16	0.12	133.5	10.9
GJ 1230 B	14.00		m	8.3	454	0.179	0.022	156	16	-0.16	0.12	133.5	10.9
LP 25-02	13.22	1.72	M4 e	14.1	1234	0.113	0.011	191	15	-0.38	0.09	71.3	16.9
G205-035	13.42		m	14.9	900	0.051	0.009	57	19	-0.34	0.16	33.0	8.8
G141-029	12.81		m	10.7	451	0.131	0.018	110	11	-0.16	0.14	98.1	13.5
Gl 725 A	8.90	1.52	dM4	3.6	1781	0.049	0.006	91	23	-0.80	0.07	19.9	0.3
Gl 725 B	9.71	1.59	dM5	3.5	1781	0.049	0.006	91	9	-0.80	0.07	19.9	0.3
Gl 725.2	4.19	0.46	F6 V	19.1	272	0.376	0.039	294	6	-0.16	0.11	280.9	122.4
Gl 726	8.81	1.29	K7	14.1	346	0.033	0.011	12	43	-1.00	0.66	9.9	2.4
Gl 727	7.97	1.07	dK4	17.3	280	0.076	0.020	22	65	-0.11	0.24	58.4	20.9
Gl 729	10.46	1.72	dM4.5e	3.0	326	0.942	0.081	334	14	-0.43	0.08	568.1	6.0
Gl 732.1	5.50	0.84	G9 IVa	26.1	785	0.415	0.024	775	6	-0.20	0.06	300.7	245.2
Gl 735	10.11	1.53	dM3 e	11.6	476	1.392	0.055	999	1	-0.20	0.04	1009.2	162.1
Gl 737 A	9.45	1.42	K7 V	12.6	115	0.092	0.032	16	74	-1.00	0.89	27.8	5.3
Gl 737 B	10.00		K5 V	12.6	115	0.092	0.032	16	74	-1.00	0.89	27.8	5.3
Wo 9638	8.09	0.91	K2	21.5	648	1.878	0.052	999	75	-0.11	0.03	1451.1	799.5
Gl 738 A	5.34	0.59	F9 V	15.0	729	0.101	0.014	97	6	-0.77	0.09	42.8	11.5
Gl 738 B	7.70		K1 V	15.0	729	0.101	0.014	97	6	-0.77	0.09	42.8	11.5
Gl 740	9.22	1.46	M2 V	11.1	442	0.029	0.010	13	35	-0.08	0.32	23.2	3.4
Steph 1676	10.60	1.42	M0	25.3	2589	0.165	0.009	765	6	-0.11	0.05	127.8	98.0
Gl 743.1A	4.87	0.52	F8 V	17.9	259	0.044	0.015	16	12	-0.74	0.28	19.3	7.4
Gl 743.1B	5.00		F8 V	17.9	259	0.044	0.015	16	12	-0.74	0.28	19.3	7.4
HD 177724	2.99	0.01	A0 Vn	25.5	435	0.141	0.020	91	41	-0.11	0.14	109.0	84.8
Gl 744	6.15	0.71	G5 IV	17.2	260	0.024	0.012	7	32			19.8	7.0
HD 177996	7.88	0.86	K1 V	31.7	215	0.421	0.046	197	5	-0.06	0.11	336.7	406.0
HD 178076	7.82		K0 V	28.8	184	0.120	0.030	28	23	-0.36	0.23	77.1	76.7
Gl 746	6.07	0.70	G5 V	21.0	450	0.047	0.012	31	24	-0.29	0.23	32.0	16.8
Gl 747 A	11.86	1.70	M3.5	8.2	701	0.025	0.007	19	2	-1.00	0.57	7.5	0.6
Gl 747 B	12.16		M5	8.2	701	0.025	0.007	19	2	-1.00	0.57	7.5	0.6
BD+79 615	9.72	1.10	dK8	32.5	1164	0.014	0.005	15	9	-0.01	0.36	11.8	14.9
Gl 748.1	5.13	0.31	F2 V	27.3	1584	0.127	0.010	351	7	-0.12	0.08	97.5	87.1
GJ 1233	7.04	0.79	G8 V	20.0	1423	0.155	0.011	360	10	-0.40	0.07	96.3	46.1
Wo 9652 A	11.55		M3	19.0	517	0.550	0.048	349	6	-0.19	0.09	401.5	174.3
Wo 9652 B	13.27		M3.5	19.0	517	0.550	0.048	349	46	-0.19	0.09	401.5	174.3
Gl 754.2	6.31	0.68	G8 V	25.3	515	0.105	0.017	105	24	-0.26	0.15	72.5	55.3
Gl 755	6.48	0.62	G5 V	20.8	291	0.627	0.049	421	12	-0.09	0.08	490.8	254.9
Gl 759	5.16	0.77	G8 IV	15.2	488	0.029	0.009	13	37	-0.62	0.34	14.4	3.9
Gl 760	3.36	0.32	F0 IV	15.4	382	0.241	0.027	185	11	-0.56	0.09	129.0	36.4
LTT 15678	13.09		m	17.9	193	0.054	0.021	12	46	-0.90	0.46	19.0	7.3
Gl 764	4.68	0.79	K0 V	5.8	1448	0.256	0.014	694	2	-0.80	0.03	104.1	4.1
Gl 765 A	4.48	0.38	F4 V	18.6	853	0.323	0.021	562	8	-0.43	0.06	195.1	80.6
Gl 765 B	13.00			18.6	853	0.323	0.021	562	8	-0.43	0.06	195.1	80.6
HD 185501	7.47		G5	32.3	415	0.032	0.011	15	23	-0.18	0.32	23.4	29.1
CD-45 13383	10.01	1.34	M1	28.8	321	0.025	0.011	10	14	-0.86	0.51	9.5	9.5
Gl 765.2	8.08	0.88	dK0	30.0	1583	0.020	0.004	22	13	-0.84	0.15	7.8	8.4
Wo 9666	5.49	0.46	F5 IV	36.6	305	0.100	0.021	47	19	-0.44	0.17	59.6	95.7
Gl 765.4A	8.35	0.99	K3 V	20.4	479	0.045	0.012	24	27	-0.85	0.20	17.2	8.5
Gl 765.4B	8.54		K3 V	20.4	479	0.045	0.012	24	27	-0.85	0.20	17.2	8.5
Gl 767.1A	4.99	0.47	F5 IV-V	20.9	468	0.136	0.018	109	6	-0.29	0.14	91.8	47.9
Gl 767.1B	8.56	1.04	dK6	20.9	468	0.136	0.018	109	33	-0.29	0.14	91.8	47.9
G125-036	12.88		m	24.4	493	0.138	0.018	128	7	-0.21	0.13	99.1	70.9
Gl 768	0.77	0.22	A7 IV-V	5.1	486	0.148	0.020	79	4	-1.00	0.06	44.5	1.4
Gl 768.1A	5.11	0.55	F8 V	19.4	401	0.046	0.013	16	22	-0.56	0.25	24.8	11.1
Gl 768.1B	13.10		M3	19.4	401	0.046	0.013	16	22	-0.56	0.25	24.8	11.1
GJ 1243	12.83	1.64	m	11.9	847	0.098	0.012	129	3	-0.26	0.11	67.9	11.5
Gl 770	6.17	1.02	K3/4 V	14.2	276	0.416	0.041	272	6	-0.48	0.09	239.8	58.1
GJ 1245 A	13.41	1.90	M5.5 V e	4.5	797	0.198	0.017	331	11	-0.37	0.08	125.8	3.1
GJ 1245 B	14.01	1.98	m	4.5	797	0.198	0.017	331	7	-0.37	0.08	125.8	3.1
Gl 771 A	3.72	0.86	G8 IV	13.7	343	0.248	0.029	202	15	-0.34	0.11	161.3	36.3
Gl 771 B	11.40		M3	13.7	343	0.248	0.029	202	15	-0.34	0.11	161.3	36.3

Name	<i>V</i>	<i>B</i> - <i>V</i>	Sp. type	<i>d</i> (pc)	Exp.	<i>CR</i>	$\pm CR$	Li	Δ	<i>hr</i>	Δhr	<i>f</i> _{x-14}	<i>L</i> _{x27}
Gl 773.2	7.90	0.80	K0 Ve	25.5	528	0.241	0.023	262	8	-0.22	0.10	172.0	133.9
Gl 773.4	5.66	0.49	F8 V	20.9	250	1.789	0.125	622	3	0.05	0.07	1534.1	799.9
HD 189733	7.67		G5	19.3	412	0.108	0.018	58	7	-0.48	0.15	62.4	27.7
Gl 775	7.46	1.14	K4 V	13.1	317	0.072	0.018	35	4	-0.74	0.17	31.8	6.5
Gl 779	5.80	0.61	G1 V	17.7	374	0.056	0.015	23	30	-1.00	0.15	16.9	6.3
GJ 1249	6.17	0.65	G5 IV	18.9	710	0.527	0.028	970	6	-0.09	0.06	412.6	175.8
Gl 780	3.56	0.76	G8 V	6.1	124	0.073	0.028	10	58	-0.52	0.41	40.5	1.8
Gl 781	11.99	1.54	dM3 e	16.5	1209	0.107	0.011	223	5	-0.42	0.09	65.4	21.2
Gl 781.1A	12.25	1.55	M3	14.6	198	0.204	0.035	60	45	-0.16	0.17	152.6	38.9
Gl 781.1B	12.50	1.63	M3.5	14.6	198	0.204	0.035	60	6	-0.16	0.17	152.6	38.9
GJ 1250	14.88	1.82	m	21.6	604	0.021	0.008	11	20	-0.35	0.33	13.7	7.7
HD 192020	7.95	0.86	G8 V	24.8	739	0.065	0.012	51	5	-0.25	0.16	45.3	33.2
Gl 784	7.97	1.43	M0 V	6.2	321	0.093	0.021	28	16	-0.67	0.19	44.1	2.0
Gl 785	5.73	0.88	K0 V	8.8	126	0.062	0.027	10	61	-1.00	0.84	18.6	1.7
Gl 786	8.88	1.33	dM0	16.8	1432	0.010	0.003	14	17	-0.52	0.23	5.8	2.0
LTT 15944	11.79		m	16.6	503	0.017	0.008	12	51	-0.58	0.24	9.0	3.0
Gl 791.1A	4.78	0.38	F2 IV	30.3	412	0.098	0.018	49	8	-0.56	0.15	52.1	57.3
Gl 791.1B	10.00			30.3	412	0.098	0.018	49	8	-0.56	0.15	52.1	57.3
Gl 791.2	13.05	1.65	dM6 e	8.8	401	0.141	0.021	85	5	-0.44	0.13	84.4	7.8
Wo 9697 A	10.28	1.34	dM1	23.1	597	0.019	0.007	12	17	-0.45	0.41	11.4	7.3
Wo 9697 B	10.70			23.1	597	0.019	0.007	12	17	-0.45	0.41	11.4	7.3
Gl 791.3	9.23	1.13	dK8	26.2	628	0.016	0.007	8	10	-0.56	0.31	8.4	6.9
Gl 793	10.56	1.56	dM3	8.0	1175	0.130	0.012	259	4	-0.45	0.08	76.9	5.8
Gl 793.1	7.09	0.79	G9 V	22.2	790	0.013	0.005	13	22	-1.00	9.99	4.1	2.4
Gl 794	11.52	-0.07	DA3	14.8	572	0.010	0.006	7	11	-1.00	2.60	3.0	0.8
Gl 795 A	8.18	1.22	K4 V	18.6	415	0.056	0.013	32	13	-0.33	0.21	36.8	15.2
Gl 795 B	9.40		K8 V	18.6	415	0.056	0.013	32	13	-0.33	0.21	36.8	15.2
GJ 1255 AB	8.00	0.86	K0 V	27.6	988	1.416	0.039	999	7	-0.05	0.03	1139.2	1040.1
GJ 1255 C	10.40			27.6	988	1.416	0.039	999	7	-0.05	0.03	1139.2	1040.1
Gl 799 A	10.99	1.57	dM4.5e	10.2	288	3.908	0.120	999	1	-0.19	0.03	2854.0	357.0
Gl 799 B	11.00		dM4.5e	10.2	288	3.908	0.120	999	1	-0.19	0.03	2854.0	357.0
GJ 1257	9.70	1.11	K5 V	23.0	169	0.525	0.057	224	16	-0.29	0.11	355.5	225.8
BD+56 2471	10.29	1.36	K7	24.0	941	0.114	0.012	178	20	-0.12	0.10	87.2	60.0
HD 197214	6.95	0.67	G5 V	22.4	427	0.027	0.011	9	21	-0.74	0.32	11.9	7.2
Gl 802	14.68	1.79	dM5 e	15.9	956	0.045	0.008	48	25	-0.42	0.15	27.7	8.3
Gl 803	8.81	1.42	M0 Ve	9.9	414	5.952	0.121	999	1	-0.08	0.02	4693.7	554.9
Gl 805	4.13	0.43	F5 V	14.7	224	0.634	0.056	408	11	-0.14	0.09	479.9	123.4
Gl 807	3.43	0.92	K0 IVe	14.3	841	0.011	0.005	10	29	-0.78	0.23	4.7	1.2
G231-017	9.74	1.32	K5	22.4	862	0.010	0.004	8	89	-1.00	0.44	3.0	1.8
HD 198809	4.58	0.83	G7 III CN	66.2	515	0.225	0.023	275	14	0.20	0.10	210.9	1106.8
Gl 809	8.55	1.48	M2 Ve	7.0	1157	0.084	0.009	139	7	-0.54	0.09	45.7	2.7
Gl 811	5.70	0.50	F8 V	21.0	375	0.389	0.034	352	5	-0.19	0.09	283.7	149.8
Gl 812 A	11.91	1.51	M3	17.7	444	0.310	0.027	303	15	-0.25	0.09	216.8	81.0
Gl 812 B	16.60	1.16	DC9+	17.7	444	0.310	0.027	303	32	-0.25	0.09	216.8	81.0
Gl 815 A	10.34	1.52	dM3 e	15.1	640	1.013	0.041	999	1	-0.24	0.04	712.9	194.6
Gl 815 B	11.90			15.1	640	1.013	0.041	999	1	-0.24	0.04	712.9	194.6
Wo 9714	9.40	1.24	K5 V	20.4	438	0.041	0.011	26	23	-0.13	0.26	31.6	15.8
G187-013	12.29		m	16.2	616	0.050	0.011	32	15	-0.65	0.17	24.1	7.6
G187-014	13.12		m	16.2	616	0.050	0.011	32	56	-0.65	0.17	24.1	7.6
Gl 816	11.23	1.49	M2.5	13.8	444	0.020	0.008	9	26	-0.78	0.33	8.2	1.9
Gl 816.1A	7.68	0.97	K2.5 V	19.3	481	0.171	0.021	130	14	-0.44	0.11	102.0	45.7
Gl 816.1B	13.00			19.3	481	0.171	0.021	130	14	-0.44	0.11	102.0	45.7
Gl 816.2A	5.10	0.17	A5 V	48.5	215	0.049	0.019	10	13	-1.00	0.35	14.8	41.8
Gl 816.2B	6.50			48.5	215	0.049	0.019	10	13	-1.00	0.35	14.8	41.8
Gl 818.1A	6.40	0.59	G3 IV	18.7	139	0.243	0.046	60	17	-0.38	0.16	153.1	64.2
Gl 818.1B	6.40			18.7	139	0.243	0.046	60	17	-0.38	0.16	153.1	64.2
Gl 818.1C	13.50			18.7	139	0.243	0.046	60	17	-0.38	0.16	153.1	64.2
Gl 819 A	7.15	0.90	K1 Ve	17.6	427	0.210	0.025	130	16	-0.42	0.11	127.7	47.5
Gl 819 B	10.20		M0	17.6	427	0.210	0.025	130	16	-0.42	0.11	127.7	47.5
Gl 820 A	5.21	1.18	K5 Ve	3.5	543	0.422	0.030	452	10	-0.72	0.05	189.5	2.8
Gl 820 B	6.03	1.37	K7 Ve	3.5	543	0.422	0.030	452	10	-0.72	0.05	189.5	2.8
Wo 9721 A	9.44	1.13	dM2	26.4	445	0.603	0.038	681	10	-0.06	0.07	482.1	401.5
Wo 9721 B	13.40	1.63		26.4	445	0.603	0.038	681	10	-0.06	0.07	482.1	401.5
Wo 9726	5.83	0.45	F7 V	32.4	464	0.119	0.018	97	12	-0.51	0.12	66.7	83.6
Gl 822.1A	3.82	0.38	F0 IV	20.9	492	0.240	0.025	210	10	-0.45	0.09	142.0	74.3
Gl 822.1B	6.42	0.60	G0 V	20.9	492	0.240	0.025	210	10	-0.45	0.09	142.0	74.3
Gl 822.1C	12.00	1.53	M3	20.9	492	0.240	0.025	210	82	-0.45	0.09	142.0	74.3
LTT 16240	12.68		m	14.4	556	0.359	0.027	506	3	-0.13	0.07	273.7	68.0
LP 341-14	13.49		m	14.4	556	0.359	0.027	506	29	-0.13	0.07	273.7	68.0
Gl 824	7.95	1.02	dK8	16.2	353	0.031	0.012	11	37	-0.46	0.29	18.3	5.7
Gl 825	6.67	1.41	M0 Ve	3.9	403	0.137	0.022	83	3	-0.73	0.10	61.0	1.1
Gl 825.1	6.60	0.68	G5 V	31.2	213	0.074	0.022	25	15	0.13	0.29	66.7	77.4
Steph 1876	12.11	1.52	M1	22.4	416	0.059	0.014	32	13	-0.35	0.22	38.2	23.0
21 14 58 -09 07.4	13.33			22.4	416	0.059	0.014	32	53	-0.35	0.22	38.2	23.0
Gl 825.2	6.75	0.63	G5 V	23.8	418	0.065	0.015	34	14	-0.46	0.20	37.9	25.7
Wo 9733 A	4.50	0.19	A5 V	29.8	317	0.419	0.040	275	6	-0.12	0.09	321.7	340.9
Wo 9733 B	6.90		A7 V	29.8	317	0.419	0.040	275	14	-0.12	0.09	321.7	340.9
Gl 826	2.44	0.22	A7 IV-V	15.0	774	0.019	0.007	11	20	-1.00	0.42	5.8	1.6
GJ 1262	6.97	0.73	G5 V	20.4	204	0.190	0.036	50	8	-0.36	0.16	121.4	60.7
Gl 831 A	12.05	1.67	dM4.5e	7.3	368	0.059	0.014	31	18	-0.52	0.22	33.0	2.1

Name	<i>V</i>	<i>B - V</i>	Sp. type	<i>d</i> (pc)	Exp.	<i>CR</i>	$\pm CR$	Li	Δ	<i>hr</i>	Δhr	f_{x-14}	L_{x27}
Gl 831 B	14.90			7.3	368	0.059	0.014	31	18	-0.52	0.22	33.0	2.1
G145-043	9.25	1.05	dK8	25.1	328	0.923	0.054	897	5	-0.15	0.06	693.9	521.5
LP 397-34	12.66		m	12.6	344	0.143	0.023	74	17	-0.33	0.15	93.7	17.9
Gl 833	7.14	0.88	K2 V	14.7	430	0.059	0.014	22	18	-0.66	0.17	28.3	7.4
Gl 834 A	10.34	1.42	dM0	21.4	657	0.113	0.015	122	10	-0.36	0.12	72.3	39.5
Gl 834 B	12.30			21.4	657	0.113	0.015	122	10	-0.36	0.12	72.3	39.5
Gl 835	9.88	1.50	M0 e	13.1	354	0.073	0.017	37	20	-0.39	0.21	45.8	9.5
Gl 836.1	6.73	0.62	G4 IV-V	25.6	367	0.090	0.019	34	14	-0.77	0.14	38.1	29.8
Gl 836.4	12.80	1.48	M1.5:	35.0	193	0.074	0.022	15	2	0.04	0.32	62.7	91.7
G093-033	12.07	1.53	dM3	21.1	356	0.062	0.016	28	4	-0.66	0.21	29.8	15.9
Gl 836.6A	4.78	0.48	F4 V	22.4	402	0.155	0.022	111	7	-0.18	0.13	113.8	68.4
Gl 836.6B	6.09		G2 V	22.4	402	0.155	0.022	111	10	-0.18	0.13	113.8	68.4
Gl 836.7	5.94	0.59	G0 V	18.4	196	0.635	0.060	296	9	-0.27	0.09	436.5	176.5
Gl 837	2.87	0.29	A6 m	11.8	345	1.655	0.125	479	4	-0.30	0.07	1112.2	185.9
GJ 1264	9.80	1.46	M2 Ve	16.1	175	0.861	0.073	355	7	-0.17	0.08	637.8	198.5
Gl 838	5.58	0.60	G2 V	15.6	334	0.067	0.017	25	8	-0.48	0.21	38.4	11.2
HD 207496 A	8.24	1.00	K3/4 V	26.4	179	0.072	0.023	23	21	-0.52	0.24	40.3	33.5
HD 207496 B	10.50			26.4	179	0.072	0.023	23	21	-0.52	0.24	40.3	33.5
Steph 1950	12.11	1.53	dM2	31.8	343	0.281	0.030	214	12	-0.19	0.11	205.4	249.2
Gl 838.5	5.08	0.37	F1 III	27.6	301	0.404	0.039	287	4	0.07	0.10	351.1	320.5
Gl 840	7.78	0.92	dK0 e	20.3	586	0.021	0.008	11	19	-0.40	0.36	12.9	6.4
G018-008	11.01	1.50	M1	19.8	327	0.035	0.013	8	8	-0.77	0.35	14.7	6.9
G188-038	12.01	1.63	m+	9.0	543	0.399	0.029	513	9	-0.22	0.07	284.8	27.4
Gl 844	10.62	1.58	M2 V	16.4	320	0.036	0.012	15	33	-1.00	9.99	10.7	3.5
Gl 845	4.69	1.06	K5 Ve	3.6	414	0.260	0.029	169	8	-0.86	0.05	97.7	1.5
G263-011	15.87	1.80	m		1086	0.010	0.004	11	3	-0.46	0.28	6.1	
Gl 848	3.76	0.44	F5 V	11.8	505	0.260	0.024	261	6	-0.58	0.07	136.1	22.5
HD 210460	6.18	0.69	G0 V	55.6	402	0.097	0.017	71	8	0.28	0.18	94.9	350.5
Gl 850	7.24	0.79	K0	22.4	554	0.075	0.013	69	5	-0.26	0.18	52.1	31.3
G188-047	13.62		m	19.8	498	0.075	0.014	50	14	-0.60	0.16	38.7	18.1
G264-022	12.90		m	16.1	627	0.015	0.006	9	24	-0.02	0.38	12.1	3.8
HD 211472	7.51	0.81	K1 V	21.5	671	0.115	0.014	118	7	-0.42	0.11	69.7	38.4
G232-062	14.00		m	21.5	671	0.115	0.014	118	76	-0.42	0.11	69.7	38.4
Gl 852 A	13.40	1.70	dM4.5e	10.0	254	0.232	0.033	148	16	-0.04	0.14	188.3	22.7
Gl 852 B	14.40	1.90	dM5 e	10.0	254	0.232	0.033	148	16	-0.04	0.14	188.3	22.7
Gl 853 A	5.39	0.60	G1 V	13.6	359	0.040	0.013	12	15	-1.00	0.15	12.1	2.7
Gl 853 B	9.90			13.6	359	0.040	0.013	12	15	-1.00	0.15	12.1	2.7
Gl 854	9.23	1.15	dK6	24.0	561	0.017	0.007	8	23	-0.73	0.42	7.6	5.2
Wo 9779	3.84	-0.05	A0 V	48.3	244	0.055	0.017	22	20	-0.44	0.25	32.9	91.8
LHS 3799	13.25	1.84	M4	7.4	271	0.158	0.026	59	13	-0.06	0.17	126.1	8.4
Gl 856 A	11.41	1.57	dM0 e	16.1	552	1.263	0.049	999	5	-0.20	0.04	915.7	283.2
Gl 856 B	11.60			16.1	552	1.263	0.049	999	5	-0.20	0.04	915.7	283.2
Gl 857.1A	8.86	1.19	dK7 e	21.4	320	0.032	0.012	16	26			26.7	14.6
Gl 857.1B	12.40			21.4	320	0.032	0.012	16	26			26.7	14.6
Gl 859 A	6.21	0.62	G3 V	20.1	274	0.847	0.058	603	3	-0.33	0.07	555.9	268.2
Gl 859 B	6.40	0.61	G3 V	20.1	274	0.847	0.058	603	14	-0.33	0.07	555.9	268.2
Gl 860 A	9.85	1.62	M2 V	4.0	427	0.449	0.034	468	7	-0.50	0.07	253.9	4.9
Gl 860 B	11.30	1.80	M6 V	4.0	427	0.449	0.034	468	7	-0.50	0.07	253.9	4.9
Gl 862.1	6.14	0.56	F7 V	25.5	193	0.031	0.015	7	39	-1.00	1.56	9.2	7.2
Steph 2018	12.41	1.57	M3	16.4	214	0.332	0.041	161	28	-0.19	0.12	242.2	77.9
Gl 863.2	5.20	0.44	F3 V	22.7	265	0.271	0.036	143	6	-0.28	0.12	185.3	114.5
Gl 863.3	7.58	0.66	G5 V	32.3	411	0.021	0.010	7	13	0.36	0.67	21.4	26.6
Gl 865	11.48	1.61	k-m	14.8	462	0.424	0.033	389	4	-0.29	0.07	286.9	75.6
Wo 9791	14.00				462	0.424	0.033	389	28	-0.29	0.07	286.9	
G189-030	9.41		M2	18.9	608	0.017	0.006	12	8	0.39	0.37	18.0	7.7
LTT 9123	10.92		m	12.9	277	0.031	0.013	9	28	-1.00	2.66	9.4	1.9
LTT 9124	12.64		m	12.9	277	0.031	0.013	9	19	-1.00	2.66	9.4	1.9
Gl 866 AB	12.66	1.98	M5 e	3.5	161	0.197	0.039	57	18	-0.50	0.17	111.4	1.6
Gl 867 A	9.10	1.51	dM2 e	8.6	225	3.803	0.187	999	10	-0.24	0.05	2676.6	239.2
Gl 867 B	11.45	1.60	dM4 e	8.6	225	3.803	0.187	999	10	-0.24	0.05	2676.6	239.2
Gl 867.1A	8.51	0.78	G8/K0 V	39.4	143	0.102	0.030	32	19	-0.08	0.31	80.8	149.9
Gl 867.1B	8.60		dG9 e	39.4	143	0.102	0.030	32	19	-0.08	0.31	80.8	149.9
Gl 868	7.82	1.13	K5 Ve	13.6	276	0.042	0.015	12	28	-0.64	0.22	20.6	4.5
Wo 9793	10.75	1.42	M0	35.7	108	0.070	0.028	16	25	-0.49	0.65	40.2	61.3
Gl 873	10.26	1.61	dM4.5e	5.0	560	5.384	0.098	999	7	-0.16	0.02	4017.5	122.5
Gl 875.1	11.63	1.55	dM3.5e	14.2	525	0.469	0.031	550	8	-0.17	0.07	347.4	84.1
Gl 879	6.48	1.10	K5 Ve	7.6	150	0.526	0.065	185	13	-0.48	0.10	303.5	21.2
Gl 880	8.67	1.50	dM2 e	6.9	419	0.036	0.011	20	17	-0.34	0.28	23.4	1.3
Gl 886.2	5.11	0.29	F0 IV	28.6	146	0.379	0.056	109	6	-0.03	0.15	309.0	301.8
GJ 1278	9.89	1.40	dM1	20.0	646	0.026	0.008	18	11	0.12	0.31	23.3	11.2
Gl 887	7.34	1.49	M2 Ve	3.3	148	0.137	0.037	28	2	-0.78	0.15	57.4	0.7
Wo 9809	10.82	1.42	dM0	24.9	598	0.549	0.032	925	29	-0.31	0.05	365.8	272.1
Gl 890	10.88	1.42	dM2.5e	21.8	138	0.427	0.059	108	14	-0.26	0.14	295.7	168.7
GJ 1279	8.39	1.20	K5 V	15.1	476	0.051	0.013	26	8	-0.47	0.20	29.6	8.0
HD 218738	7.91	0.90	G5	29.3	408	1.928	0.070	999	7	-0.12	0.04	1479.5	1522.3
Gl 892	5.56	1.01	K3 V	6.5	497	0.023	0.009	10	32	-0.96	0.18	7.4	0.4
GJ 1282	5.66	0.51	F7 V	20.6	374	0.635	0.043	560	7	-0.01	0.07	524.7	265.8
HD 219509	8.73	1.05	K5 V	27.2	449	0.030	0.010	11	60	-0.54	0.28	16.6	14.8
HD 219495	9.04	1.11	K5 V	27.1	449	0.030	0.010	11	12	-0.54	0.28	16.6	14.6
Wo 9818	3.99	0.40	F1 III	22.0	339	0.097	0.020	42	4	-0.72	0.13	43.7	25.4

Name	V	$B - V$	Sp. type	$d(\text{pc})$	Exp.	CR	$\pm CR$	Li	Δ	hr	Δhr	f_{x-14}	L_{x27}
G067-053	12.10	1.59	M4		418	0.323	0.030	303	13	-0.40	0.08	199.8	
BD+08 5036	9.72	1.13	dK8	37.0	419	0.032	0.011	15	22	-0.24	0.35	22.5	36.8
HD 219693	5.53	0.44	F5 V	34.6	145	0.063	0.025	12	8	0.44	0.39	66.7	95.6
GJ 1283	8.97	1.15	K4 V	19.2	313	0.035	0.014	8	26	-0.63	0.27	17.3	7.7
G1 894.2A	5.20	0.79	G5 IV	20.7	304	0.036	0.013	13	20	-0.79	0.32	14.8	7.6
G1 894.2B	7.61	0.91	K2 V	20.7	304	0.036	0.013	13	21	-0.79	0.32	14.8	7.6
G1 894.4	7.36	0.80	K1 V	21.9	432	0.148	0.020	102	10	-0.49	0.12	84.5	48.6
G1 895	10.04	1.50	dM2 e	13.1	514	0.015	0.007	8	8	-0.58	0.34	7.9	1.6
LHS 543a	14.59	1.66	m	24.8	405	0.054	0.013	32	27	0.14	0.26	48.6	35.6
G190-028	11.87	1.52	M2	14.9	263	0.812	0.057	612	28	-0.34	0.07	528.8	140.1
G190-027	12.44	1.61	M3 :	14.7	263	0.812	0.057	612	16	-0.34	0.07	528.8	136.8
GJ 1284	11.16	1.51	M2 Ve	16.1	299	0.500	0.043	426	2	-0.20	0.09	362.6	112.8
HD 221239	8.31	0.93	K0	25.6	764	0.017	0.006	11	27	-0.76	0.25	7.3	5.8
G1 896 A	10.38	1.54	dM4 e	6.2	17	0.993	0.250	37	80	0.05	0.25	851.3	39.7
G1 896 B	12.40	1.65	dM6 e	6.2	17	0.993	0.250	37	80	0.05	0.25	851.3	39.7
G1 897 A	10.95	1.51	M3.5	15.4	315	0.888	0.055	800	6	-0.28	0.06	606.0	172.7
G1 897 B	11.40			15.4	315	0.888	0.055	800	6	-0.28	0.06	606.0	172.7
G1 898	8.60	1.28	K5/M0 V	13.9	313	0.104	0.021	48	8	-0.57	0.15	55.1	12.8
G1 900	9.56	1.35	dM0.5	19.3	374	0.320	0.031	278	1	-0.13	0.09	243.9	108.8
HD 221851	7.91	0.84	K0	23.5	596	0.030	0.009	18	10	-0.48	0.23	17.4	11.5
CP-49 11759	10.09	1.37	M0	23.8	146	0.531	0.061	182	37	-0.20	0.12	384.8	259.8
BPM 45048	12.37	1.44		23.8	146	0.531	0.061	182	37	-0.20	0.12	384.8	259.8
W _o 9832	3.82	1.01	G8 III-IV	25.8	364	9.822	0.164	999	5	-0.07	0.02	7797.6	6229.1
HD 222143	6.58	0.66	G5	23.1	344	0.286	0.030	239	5	-0.36	0.10	183.2	116.9
CD-42 16413	11.93	1.46	M3	18.5	78	0.060	0.030	8	43	-1.00	1.58	18.0	7.3
G068-034	14.24		m	23.3	338	0.035	0.012	10	15	-0.87	0.31	12.9	8.3
LP 463-28	17.90		g	23.3	338	0.035	0.012	10	9	-0.87	0.31	12.9	8.3
G1 902	7.07	0.99	K3 V	11.4	462	0.029	0.010	12	11	-1.00	0.44	8.8	1.4
G1 903	3.21	1.03	K1 IVe	13.8	977	0.014	0.005	12	8	-0.78	0.27	5.9	1.3
G1 904	4.13	0.51	F7 V	13.8	373	0.111	0.019	73	5	-0.89	0.07	40.1	9.1
G1 905	12.29	1.90	dM6 e	3.2	350	0.177	0.024	100	5	0.15	0.14	161.3	1.9
W _o 9836 A	4.48	-0.04	B9 V	47.2	272	0.583	0.048	377	10	-0.12	0.08	447.5	1191.2
W _o 9836 B	11.00			47.2	272	0.583	0.048	377	10	-0.12	0.08	447.5	1191.2
GJ 1289	12.57	1.60	k	8.1	453	0.105	0.018	79	15	-0.45	0.14	62.2	4.9
G241-068	11.30	1.40	M1.5	28.9	581	0.317	0.025	400	9	-0.30	0.07	212.8	212.7
GJ 1290	13.30	1.59	m	22.0	322	0.112	0.020	83	3	-0.11	0.17	86.5	50.2
G273-130	14.50		m	9.0	126	0.078	0.031	9	35	-0.39	0.32	48.8	4.7
G1 907.1AB	9.86	1.26	dM0	27.0	353	0.404	0.035	327	11	-0.24	0.09	284.5	248.7
G275-106	12.40		M3.5:	18.5	301	0.187	0.027	79	7	-0.32	0.14	123.5	50.7
G1 908	8.98	1.48	M2 Ve	6.0	414	0.051	0.013	27	10	-0.31	0.23	34.1	1.5
G029-069	13.57		dM4 :	20.8	432	0.050	0.013	21	11	-0.84	0.17	19.1	9.9
G1 908.1	9.34	1.26	dK8	24.9	299	0.034	0.013	12	55	-1.00	1.04	10.3	7.6
G1 909 A	6.40	0.98	K3 V	10.8	747	0.419	0.025	795	9	-0.40	0.05	259.4	36.1
G1 909 B	11.70		M2	10.8	747	0.419	0.025	795	9	-0.40	0.05	259.4	36.1
HD 224085	7.38	1.01	K1 V	42.4	277	10.900	0.200	999	1	-0.15	0.02	8191.3	17596.3
HD 224228	8.21	0.96	K3 V	22.1	133	0.116	0.035	20	11	-0.30	0.28	77.8	45.3
G273-186	12.93		M4	16.5	331	0.256	0.030	130	9	-0.30	0.11	172.1	56.1
G273-185	12.98		M4	16.5	331	0.256	0.030	130	13	-0.30	0.11	172.1	56.1
LP 291-34	12.64		m	18.0	331	0.228	0.027	160	7	0.05	0.12	195.4	75.9
HD 224635	6.47	0.55	F8 V	29.0	306	0.159	0.024	87	3	-0.62	0.12	80.0	80.4
G1 914 A	5.81	0.67	G3 V	12.4	369	0.029	0.011	12	30	-0.45	0.32	17.2	3.2
G1 914 B	9.00		K6 V	12.4	369	0.029	0.011	12	30	-0.45	0.32	17.2	3.2